

# *Reflective Hard X-ray Optics: Recent Developments for Astrophysics and Free Electron Lasers*



Joint Instrumentation Seminar

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# X-RAY OPTICS PRIMER



# X-ray optics can use a wide range of phenomena

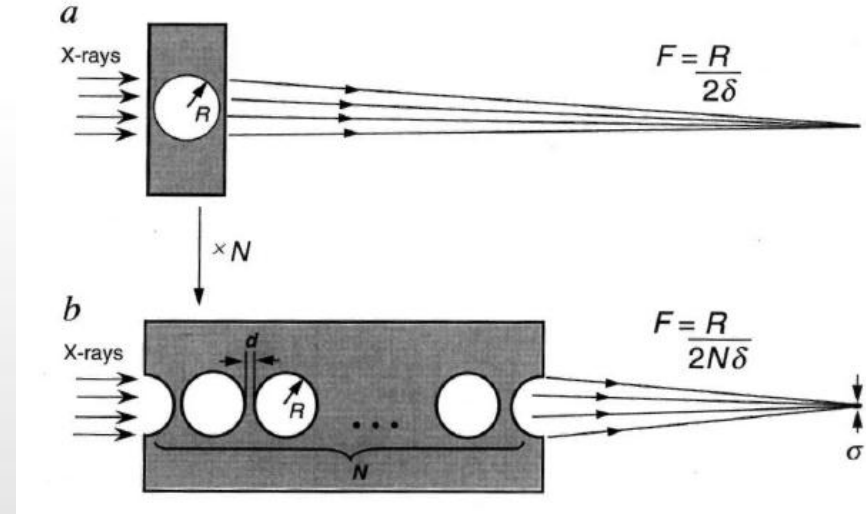
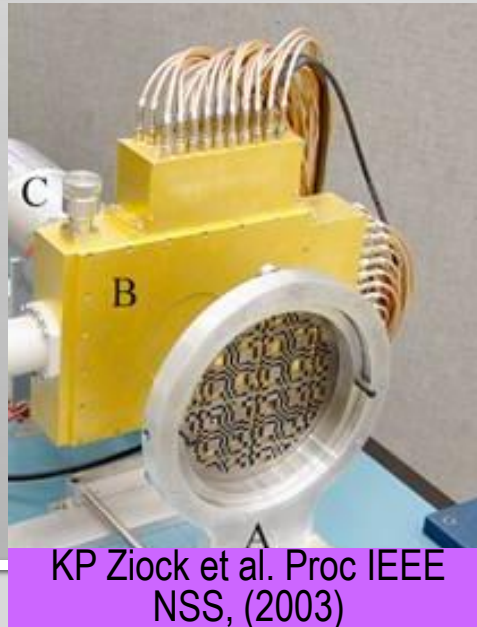
## Diffraction

- Gratings
- Fresnel zone plates



## Absorption

- Pinholes
- Anger cameras
- Coded apertures



A Snigirev et al. *Nature*, 384, 49, (1996)

## Refraction

- Compound refractive lens

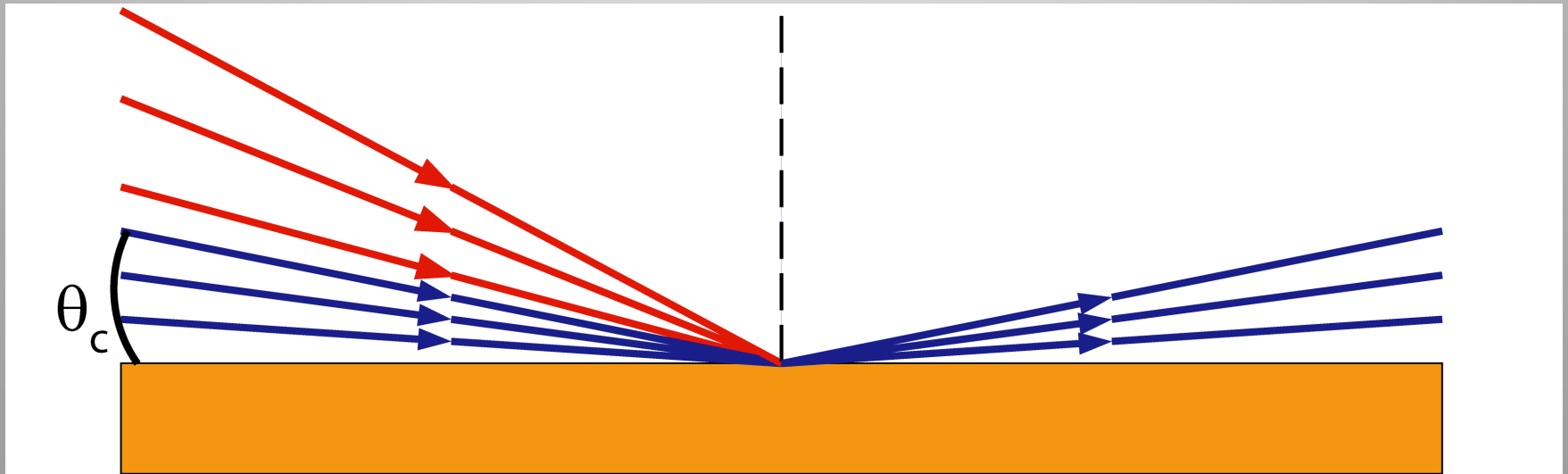
## Reflection

- Capillary optics
- Mirrors

Today's seminar

# Reflective x-ray optics

- Compton first discovered X-rays incident at small glancing angles are totally reflected
  - “The Total Reflexion of X-rays”, *Philosophical Magazine*, **45**, 1121, (1923)
- Index of refraction for high energy photons  $n = 1 - \delta - i\beta$
- Total external reflection of light occurs when the incident angle is less than the critical angle  $\theta_c = \sqrt{2\delta}$ .
- Critical angle drops rapidly with energy  $\theta_c \sim E^{-1}$ .



# Original reflective x-ray optic concepts

“Formation of Optical Images by X-rays”

P Kirkpatrick, AV Baez

*J Opt Soc Amer*, 38, 766, (1948)

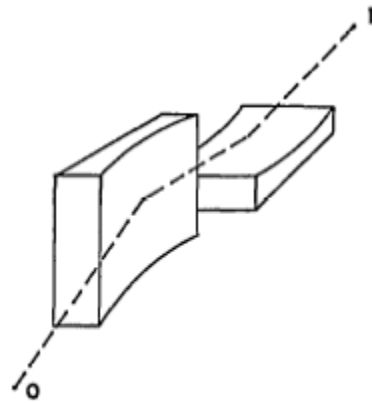


FIG. 11. Arrangement of concave mirrors to produce real images of extended objects with incidence at small grazing angles.

- Two (or more) concave, spherical mirrors
- Does not meet the Abbe sine rule

“Spiegelsysteme streifenden Einfalls als abbildende Optiken für Röntgenstrahlen”

H Wolter, *Phys Ann* 10, 94, (1952)

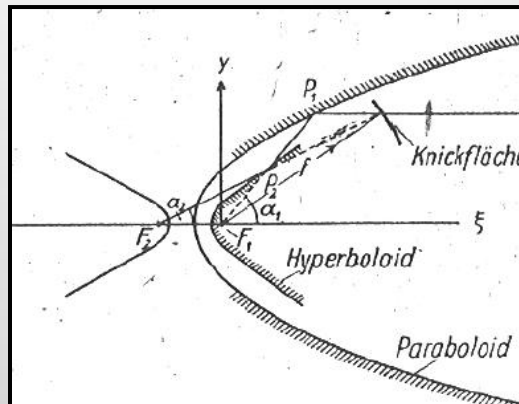


Abb. 15. Spiegelsystem 2. Art

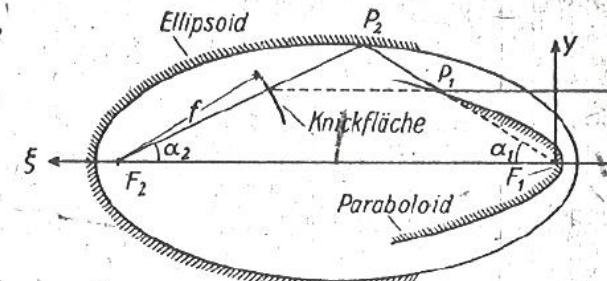


Abb. 16. Spiegelsystem 3. Art

- Even number of conic surfaces of revolutions (hyperbola+parabola, hyperbola+ellipse, etc.)
- Nearly satisfies Abbe sine rule
- Significant increase in solid angle (compared to KB)

# Wolter optics for x-ray astronomy

- Wolter originally proposed his designs for an x-ray microscope for biology
  - Not possible to fabricate
- Idea later adopted by Giacconi *et al.* for astronomy



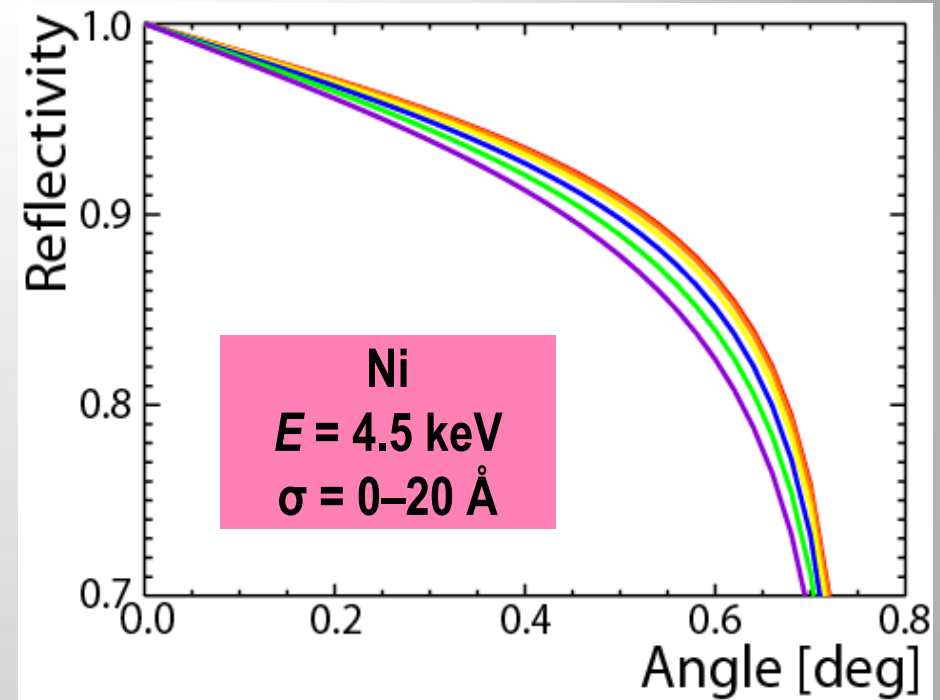
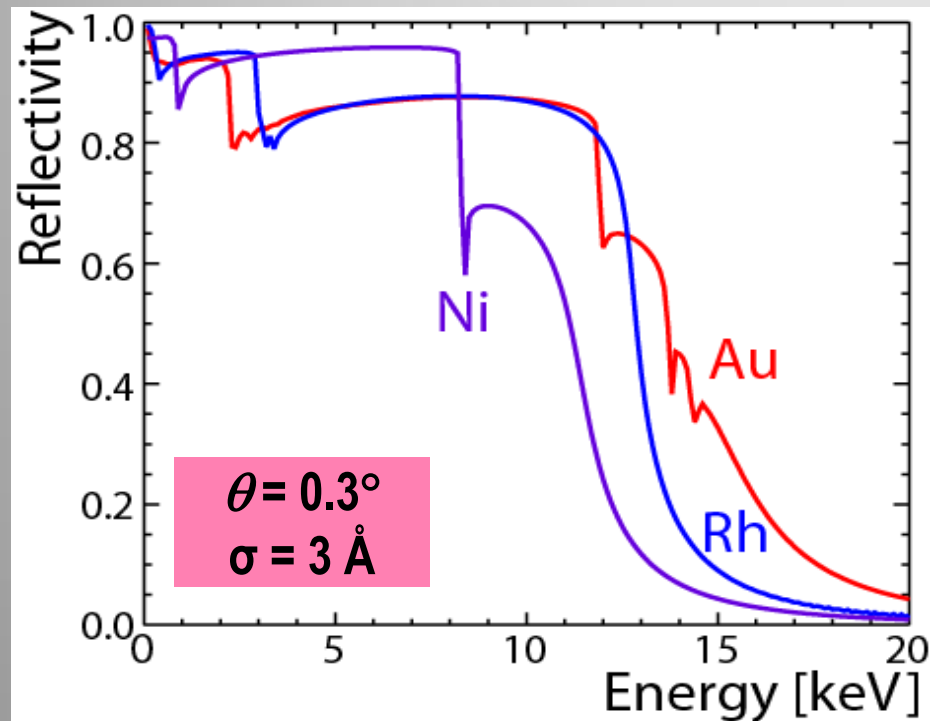
- Key innovation was the realization that mirrors could be nested inside one another to increase collecting area (solid angle)



# X-ray reflectivity

Limited to materials that:

- can be polished well or deposited smoothly (*e.g.*, Ni, Rh, Au, Ir)
- do not have absorption edges in operational band



- Reflectivity depends not only on material, but also its high-spatial frequency roughness (*i.e.*, finish)

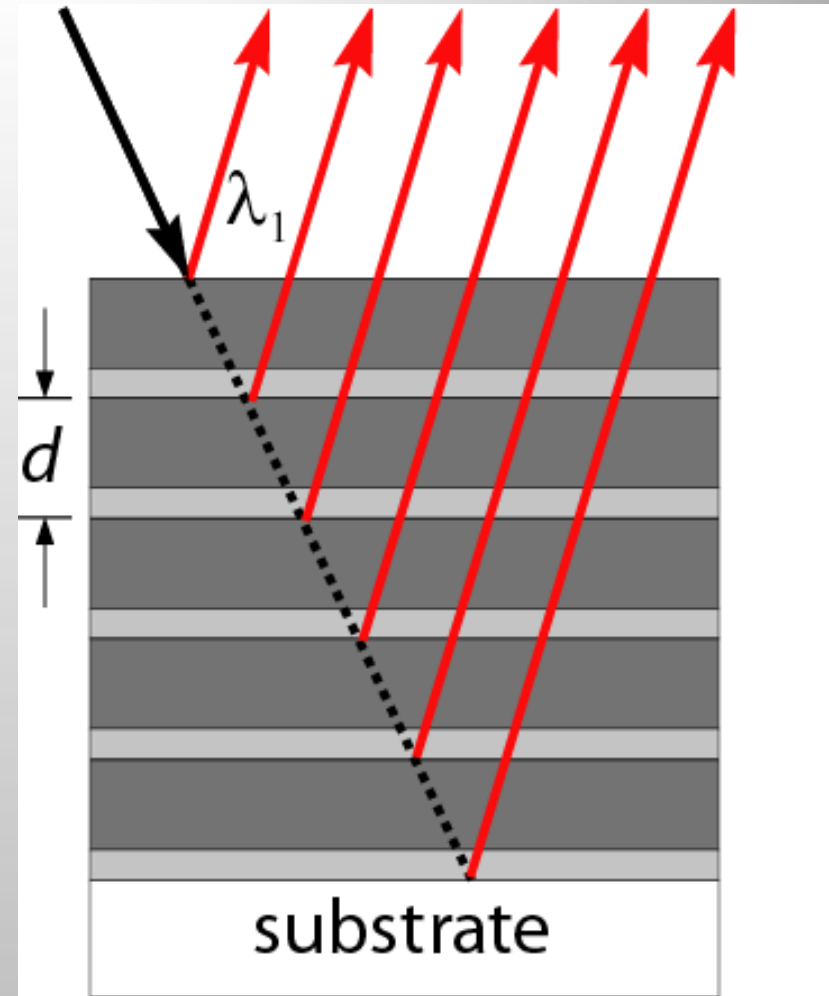


# X-ray multilayers

- At high energies, graze angles ( $\theta_c$ ) become too shallow for efficient optics: switch to **multilayers**
- Alternating layers of high- and low-Z materials act as reflecting interfaces, following Bragg's law

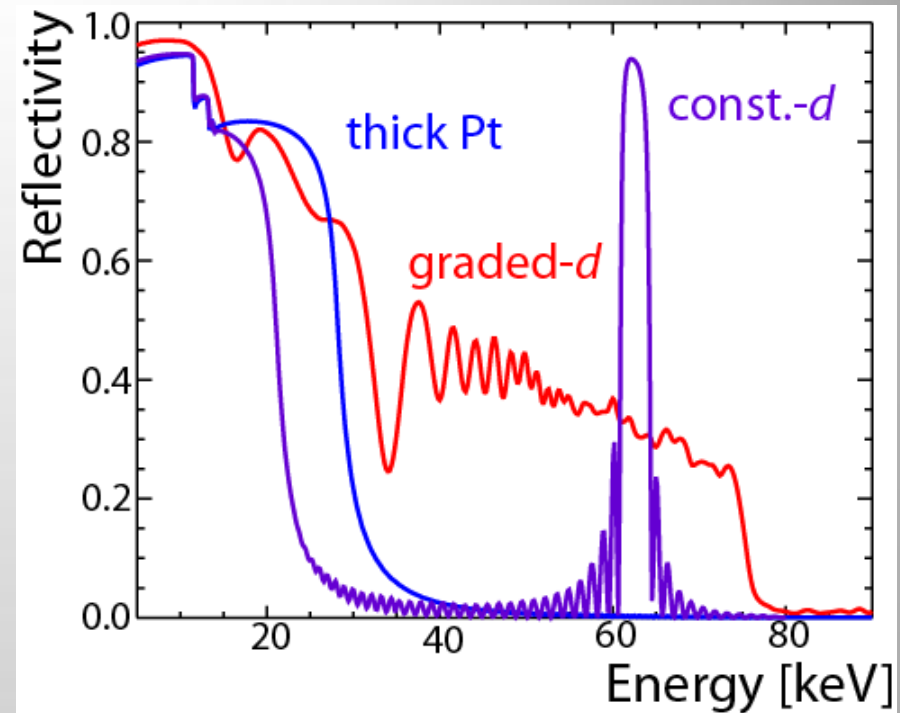
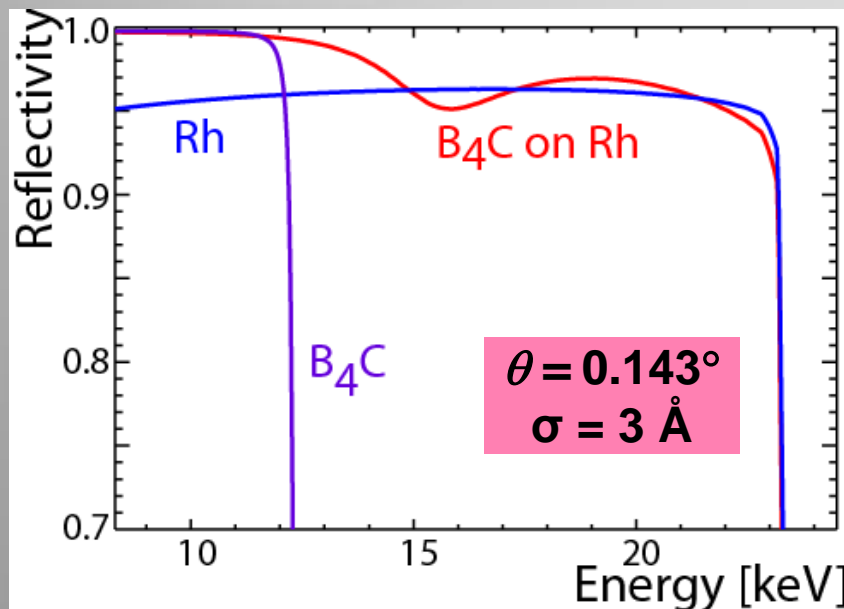
$$m\lambda = 2d \sin \theta \sqrt{1 - \frac{2\delta}{\sin^2 \theta}}$$

- Theory described in 1920s-1930s
- First proposed for X-ray applications in early 1970s by Spiller *et al.*
- Initially, constant- $d$  designs used for high reflectivity for particular bands
- Later, Christensen *et al.* proposed [*Proc SPIE*, **1736**, 229, (1992)] varying  $d$ , to satisfy the Bragg equation over a range of  $\theta$  and  $\lambda$  ( $\sim 1/E$ ) at high energies.



# Multilayer performance

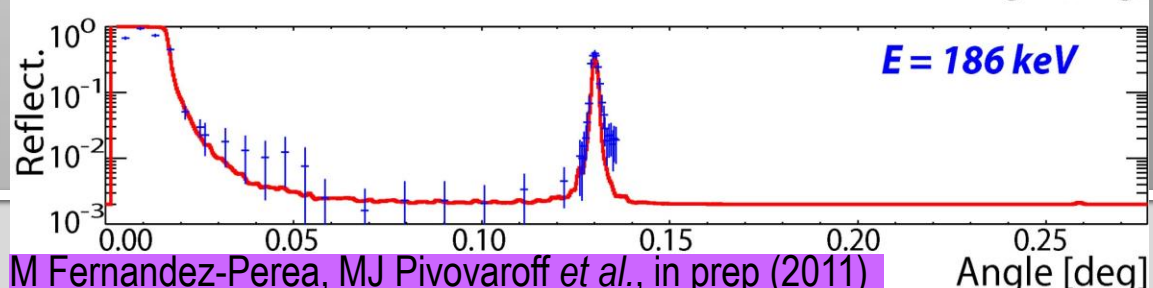
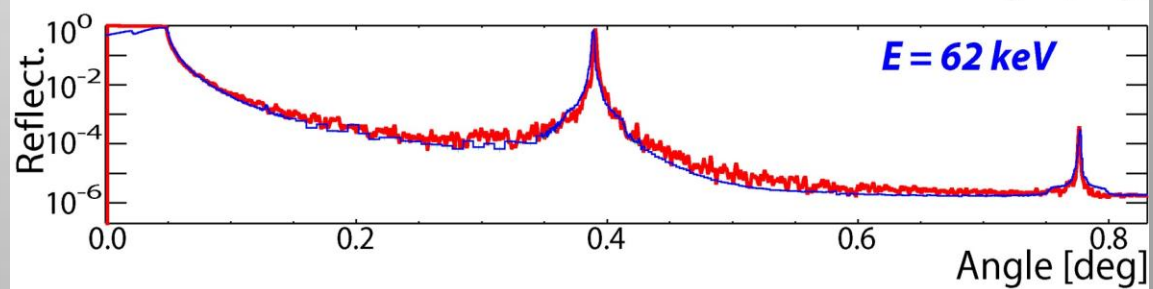
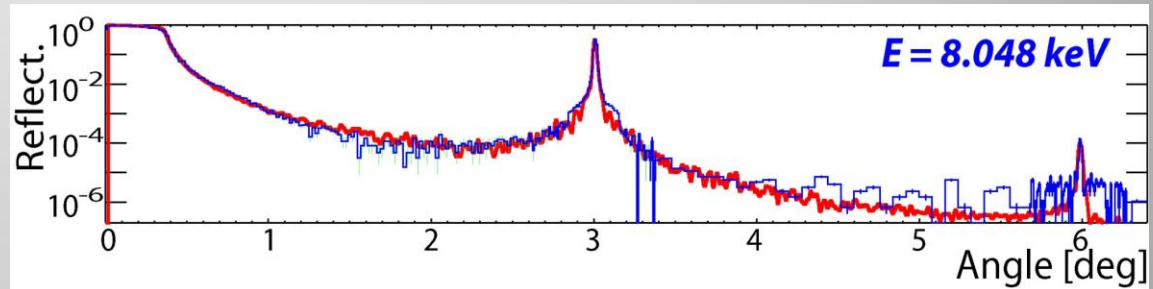
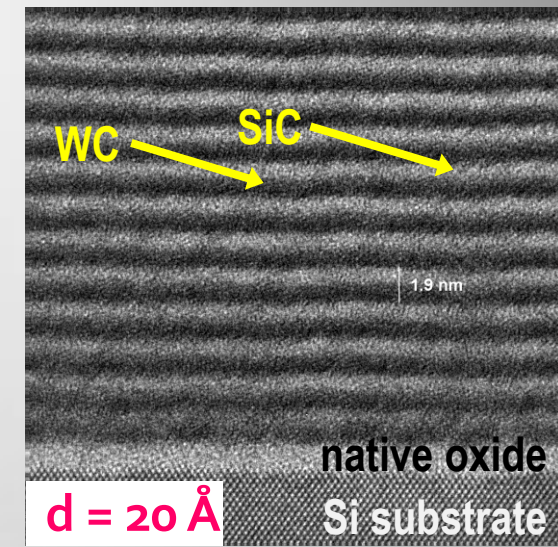
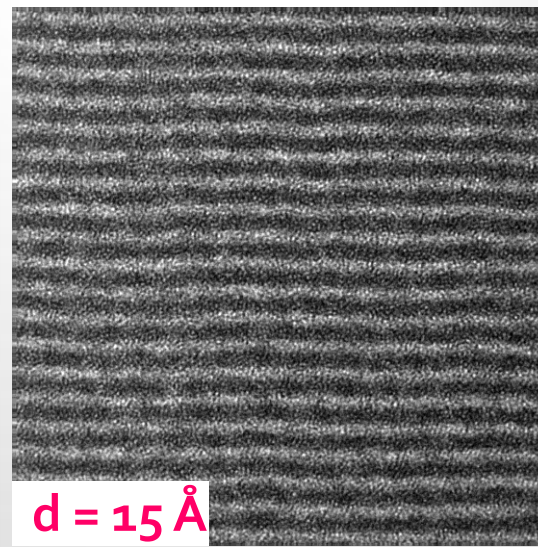
- Recipes can be tuned for application; tremendous versatility
- Systems can consist of 1000's of bilayers to just a few layers ("overcoatings")
- Practically, limited by absorption, stress, absorption, material properties and other constraints (cost, time)



- Semi-infinite Pt coating with  $\sigma=3\text{\AA}$
- Constant-d: Pt/SiC,  $\sigma=3.0\text{\AA}$ ,  $N=90$ ,  $d=35\text{\AA}$   $\Gamma=0.56$
- Graded-d: Pt/SiC,  $\sigma=4.5 \text{ \AA}$ ,  $N=566$

# How high can you go in energy?

- Several groups have published reflectance measurements from multilayers above 100 keV
  - Windt et al; Jensen et al;
  - High reflectivity reported; some discrepancies between measurements and theoretical values
- We have recently fabricated WC/SiC multilayers with periods of 10-20 Å and  $N = 300-500$  and tested them at NSLS at 186 keV
  - Excellent agreement between model and data

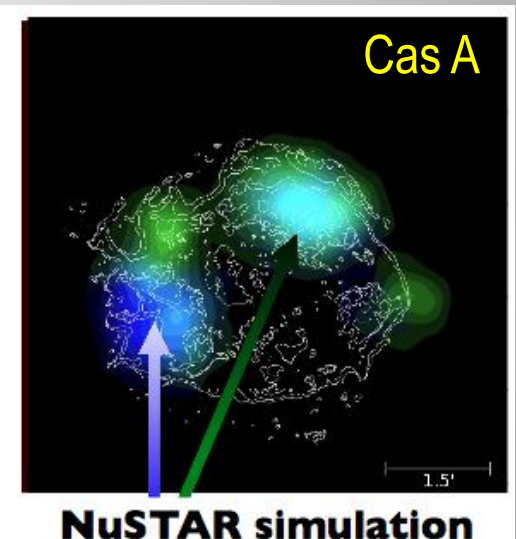
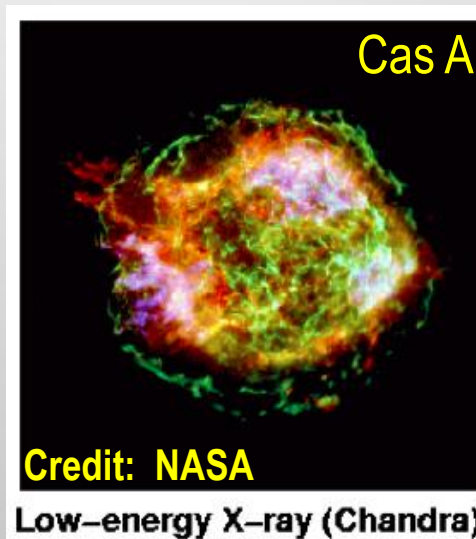


# NUSTAR



# Hard x-ray astrophysics

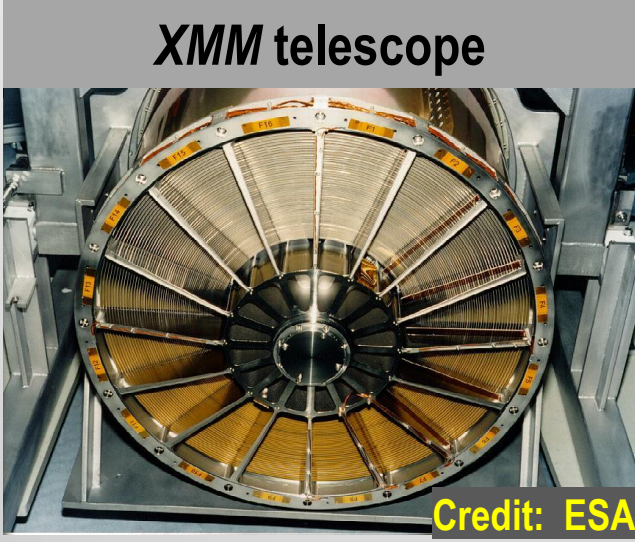
- Want to make observations above  $\sim 10$  keV where traditional x-ray mirrors (i.e. those coated with a simple metal reflective layer) lose effectiveness
- Why?
  - Nucleosynthesis: observe young supernova remnants like Cas A
  - Black hole surveys
  - Extragalactic science (e.g, blazars)
  - Compact objects (e.g., neutron stars)



# Moving from the soft x-ray band ...

## XMM-Newton; ESA

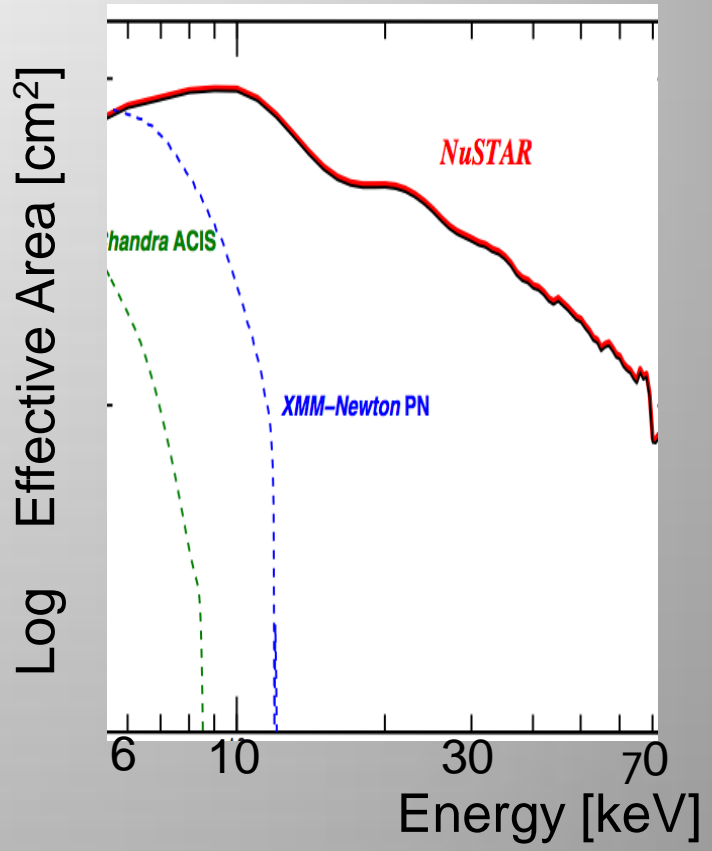
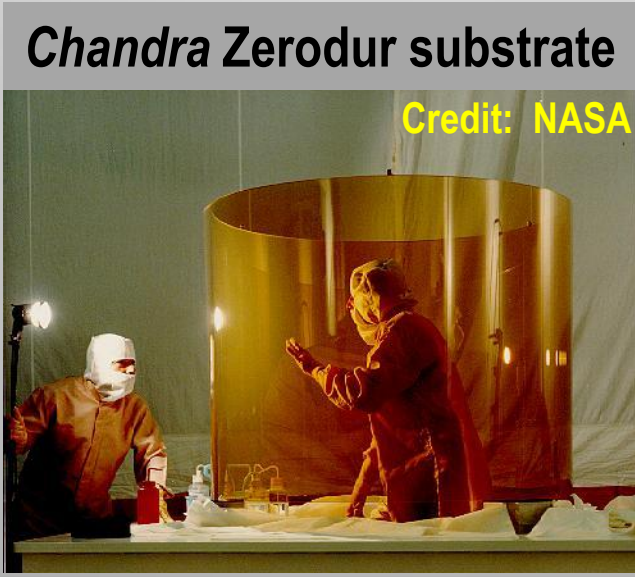
- 15" HPD
- 3 telescopes, 58 nested shells
- 120 m<sup>2</sup> surface area
- Mirrors: 200M DM (\$120M US)
- Total: \$700M US
- Replicated from precision mandrels



**NuSTAR requires large area above 10 keV**  
**How do we do it within a SMEX program?**

## Chandra; NASA

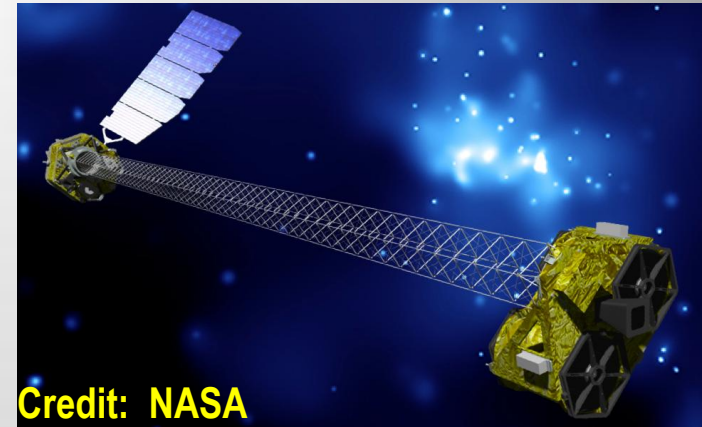
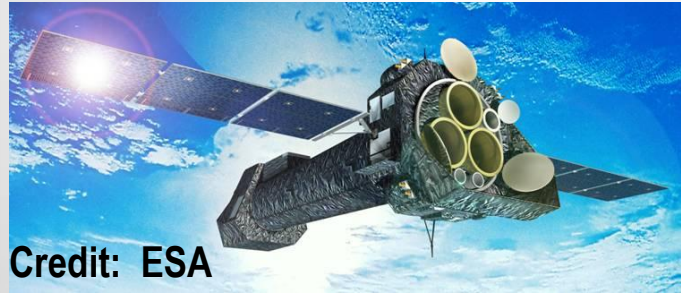
- 0.5" HPD
- 1 telescope, 4 nested shells
- 10 m<sup>2</sup> surface area
- Mirrors: \$700M US
- Total: \$1600M US
- Polished monolithic blanks



# ... into the hard x-ray band with NuSTAR

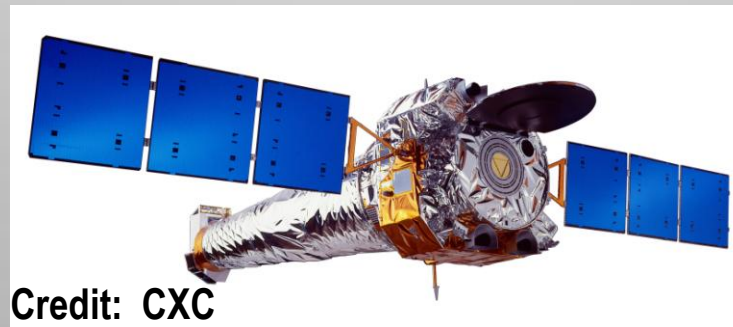
## XMM-Newton; ESA

- 15" HPD
- 3 telescopes, 58 nested shells
- 120 m<sup>2</sup> surface area
- Mirrors: 200M DM (\$120M US)
- Total: \$700M US
- Replicated from precision mandrels



## Chandra; NASA

- 0.5" HPD
- 1 telescope, 4 nested shells
- 10 m<sup>2</sup> surface area
- Mirrors: \$700M US
- Total: \$1600M US
- Polished monolithic blanks



## NuSTAR

- 45" HPD goal
- 2 telescopes, 130 nested shells
- 80 m<sup>2</sup> surface area
- Mirrors: \$10–15M US
- Total: \$100M US
- **Thermally-formed, multilayer-coated mirrors**

# Solution: glass substrates

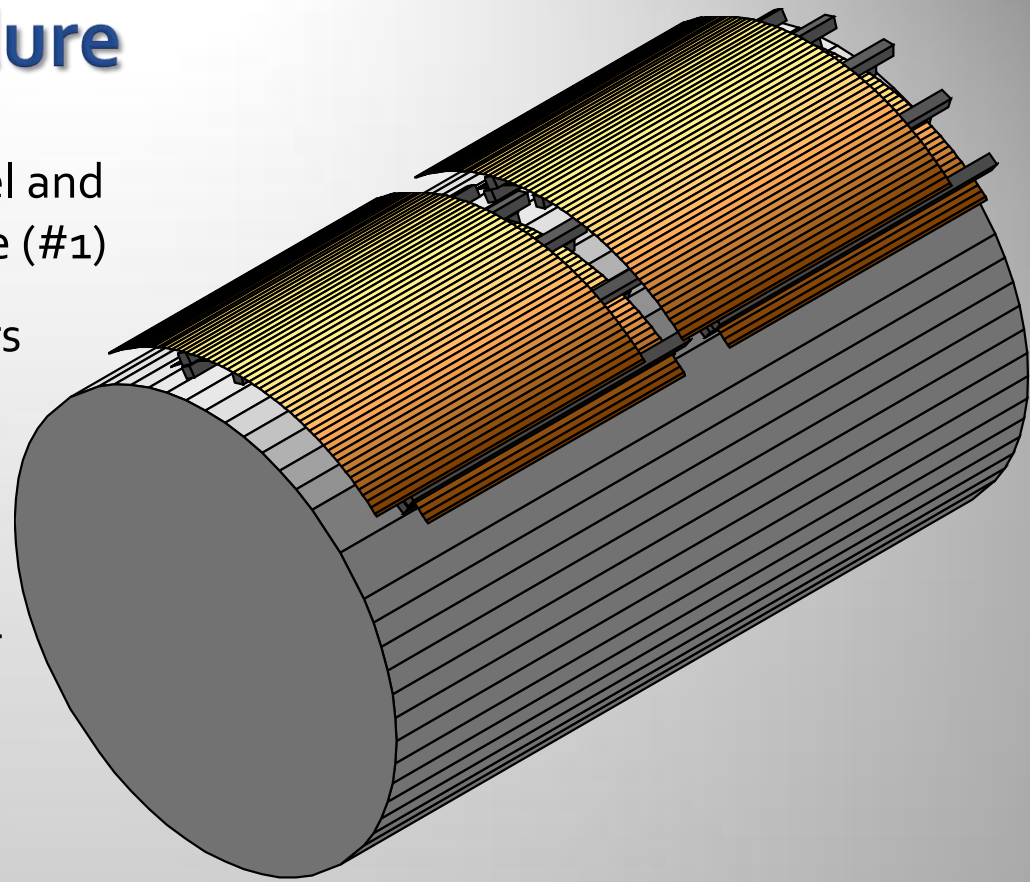
- Work dates back as far as 1988
  - Labov, *Applied Optics*, **27**, 1465, (1988).
- Columbia/DTU/LLNL starts in earnest in late 1990's for the High Energy Focusing Telescope (HEFT) balloon mission
- Start with flat panel float glass (Schott and Corning) which has nice thickness uniformity and excellent surface finish (roughness  $\sigma = \text{few } \text{\AA}$ )
- Thermally form ("slump") into near net shape
  - Take flat pieces of glass and turn into cylindrical shapes
- Coat with appropriate reflective coatings
- Assemble into an optic



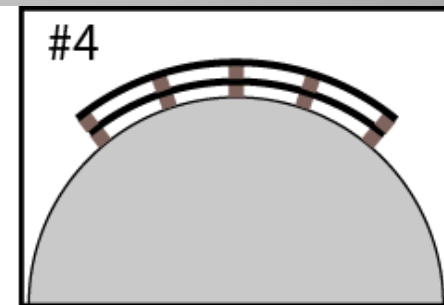
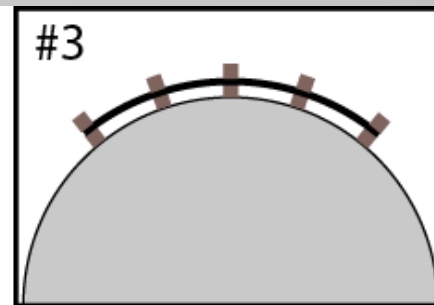
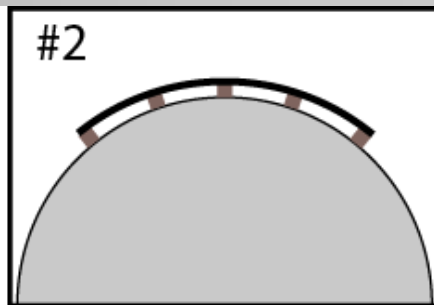
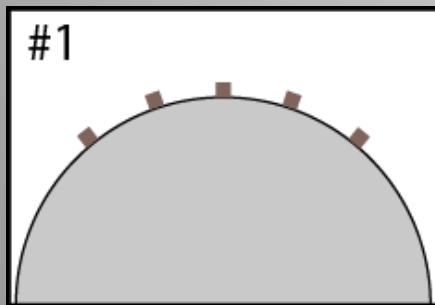


# Optics assembly procedure

- Epoxy graphite spacers onto a mandrel and machined to the correct radius & angle (#1)
- Epoxy ML-coated substrates to spacers (#2)
- After epoxy cures, epoxy next layer of spacers to previous layer of glass (#3)
- Machine these spacers, epoxy another layer of glass into place (#4)
- Repeat until entire optic is assembled



J.E. Koglin et al., *Proc. SPIE*, **4851**, 607, (2003)



# HEFT optics

diameter = 80 mm

HF1

diameter = 240 mm

HF2

HF3

- Three optics built during ~2 year fabrication cycle (4400 mirror segments)

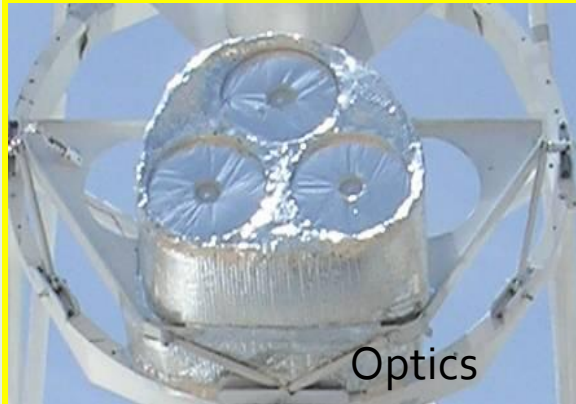
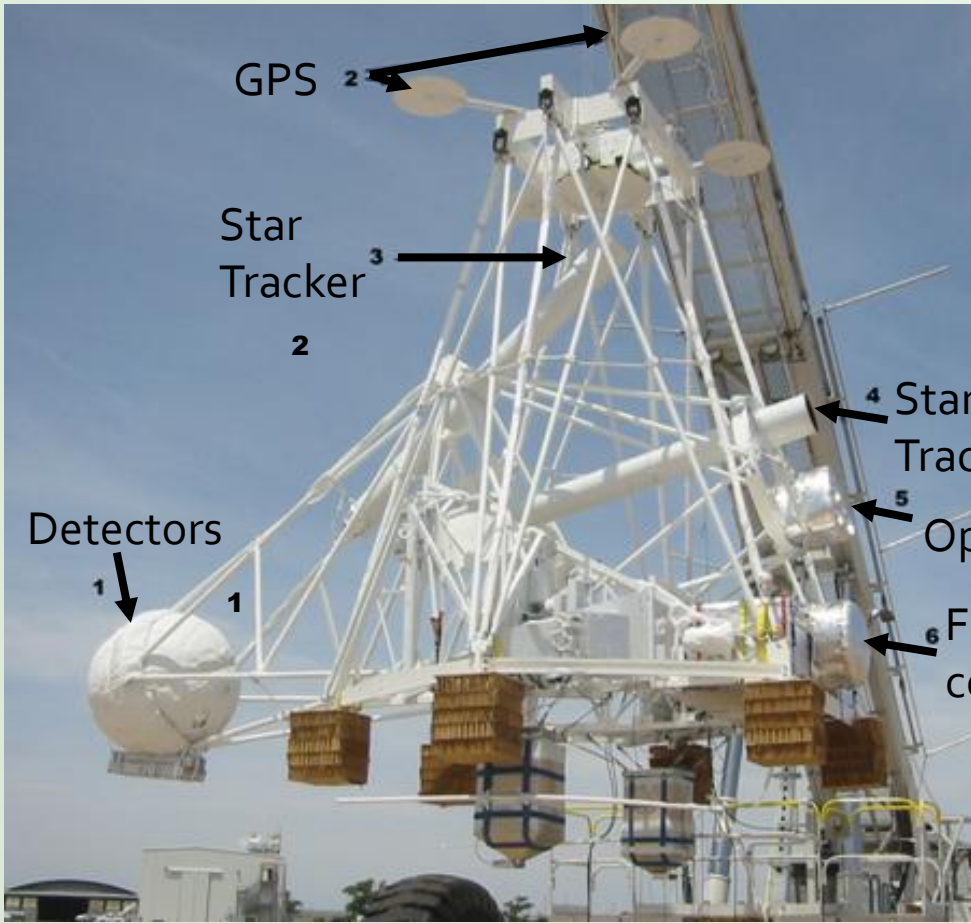
Caltech, Columbia, DSRI (DNSC) & LLNL

- In flight performance: 60–80" HPD
- Prototype resolution: 43" HPD
- HEFT flight module (72 layers)

J.E. Koglin *et al.*, *Proc SPIE*, **5168**, 100, (2004)

J.E. Koglin *et al.*, *Proceedings of The X-ray Universe 2005*, 955, (2006)

# HEFT ready for launch (summer 2005) New Mexico



F.A. Harrison *et al.*, *Experimental Astronomy*, **20**, 131, (2005)



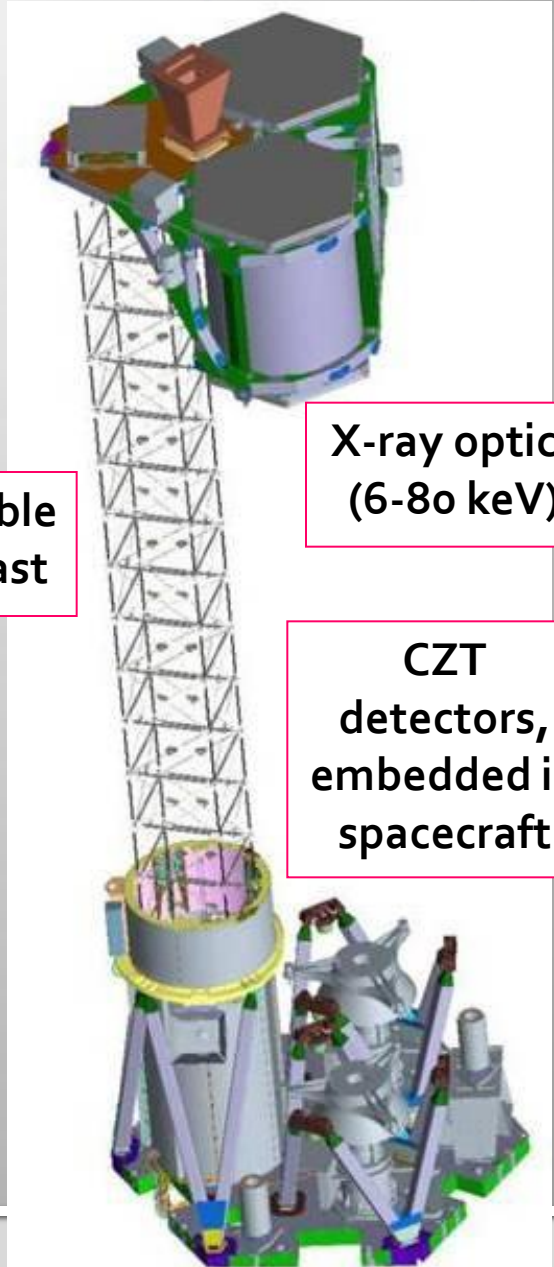
# NuSTAR (Nuclear Spectroscopic Telescope Array)

- NuSTAR starts in 2004 (PI Fiona Harrison, Caltech)
  - Leverages *HEFT* technology development
- NASA SMEX mission (\$100M, not including launch); launch scheduled for 3 Feb 2012
- First focusing x-ray optics above 10 keV
  - order of magnitude more sensitivity than previous missions
  - CdZnTe focal plane array for extremely good spectroscopy ( $\Delta E < 1$  keV)

Extendable  
10-m mast

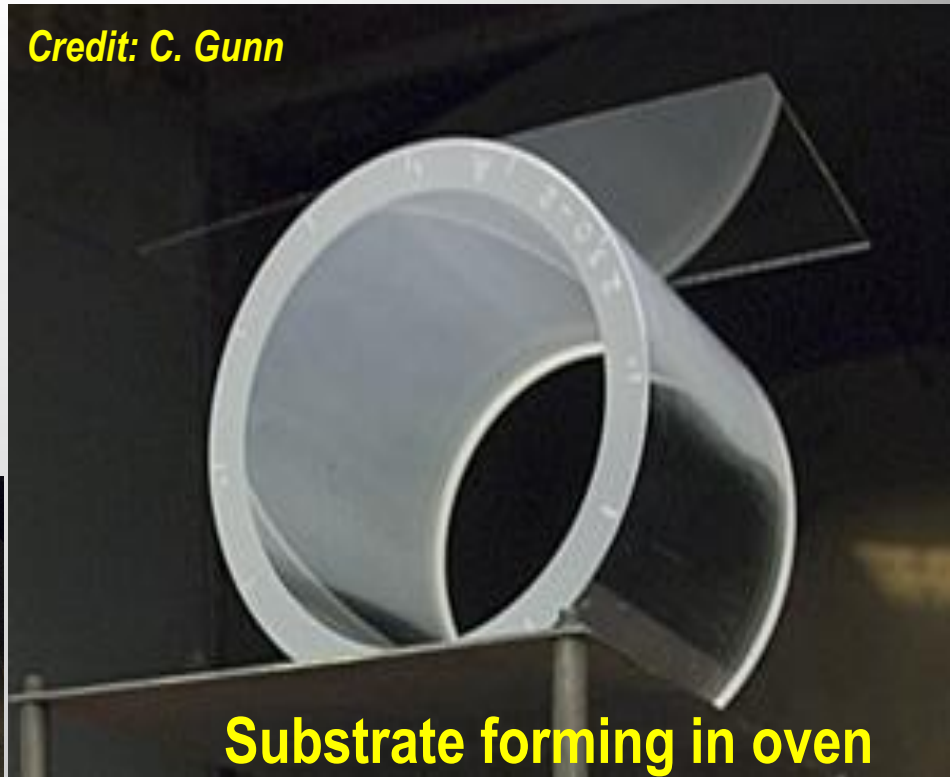
X-ray optics  
(6-80 keV)

CZT  
detectors,  
embedded in  
spacecraft



# Optics start with thermally forming substrates

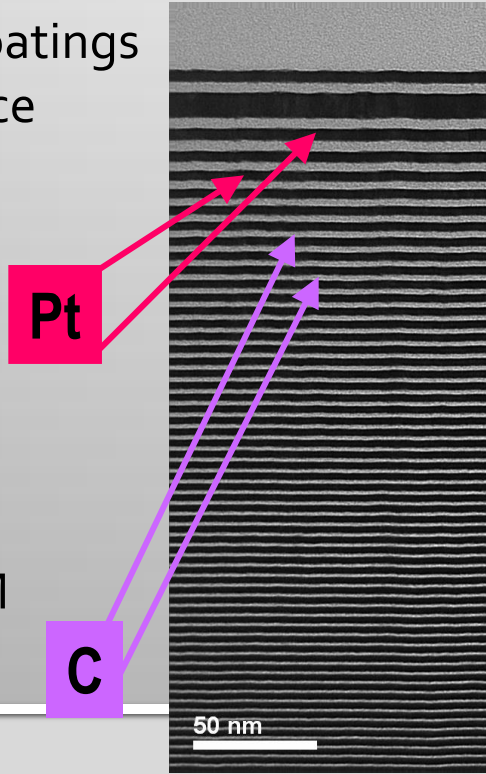
- Optics PI, Charles Hailey, Columbia University
- Team includes: Columbia U., DTU-Space, NASA GSFC, LLNL



- GSFC approach slumps glass directly onto highly polished mandrels
- Excellent figure (10–20" HPD) has been demonstrated

# Depth-graded multilayer coatings provide broad band response

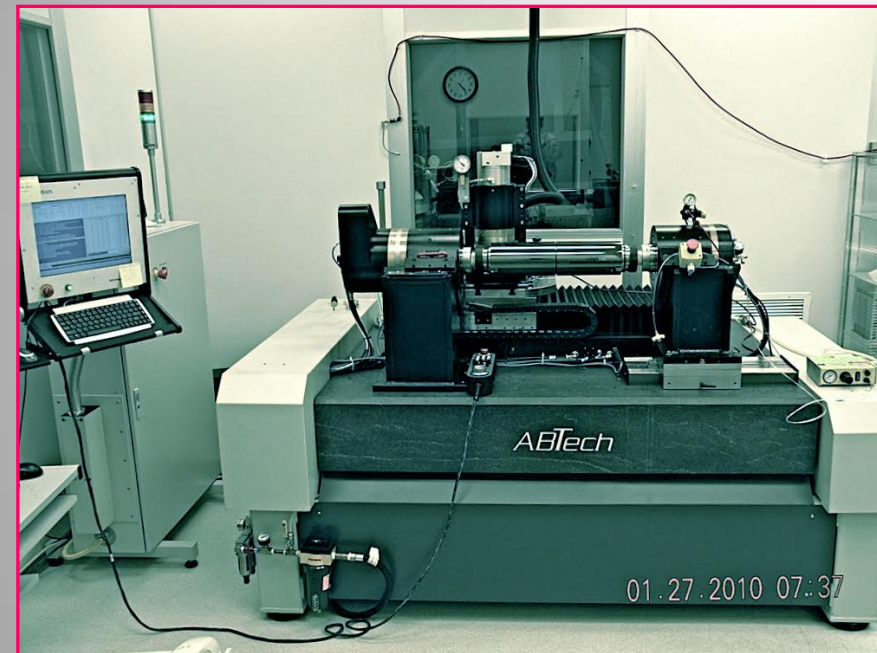
- Two material systems used, driven by need to detect Ti-44 lines at 68 & 78 keV
  - Pt/C provides highest response
  - W/Si less expensive and smoother
- 10 different multilayer recipes used
- X-ray testing to optimize coatings and understand performance
  - 8 keV (DTU)
  - 60 keV (NSLS)
  - 10-90 keV (RaMCaF)
- Extensive metrology to validate models
  - Surface roughness, TEM compositional studies



F Christensen et al., Proc SPIE, 8147, (2011)



# NuSTAR telescopes assembled at the Nevis Laboratories, Columbia University



Two custom-built assembly machines are used to precisely mount the glass segments at Columbia's Nevis Laboratory

J Koglin *et al.*, *Proc SPIE*, **8147**, (2011)  
W Craig *et al.*, *Proc SPIE*, **8147**, (2011)



Glass is positioned and clamped for overnight cure of epoxy

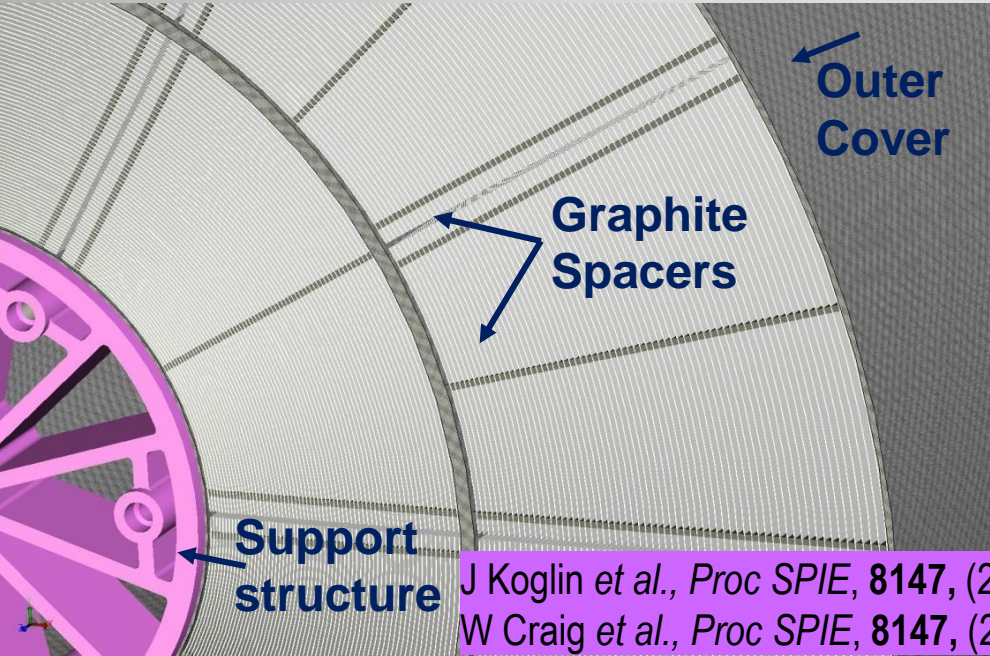
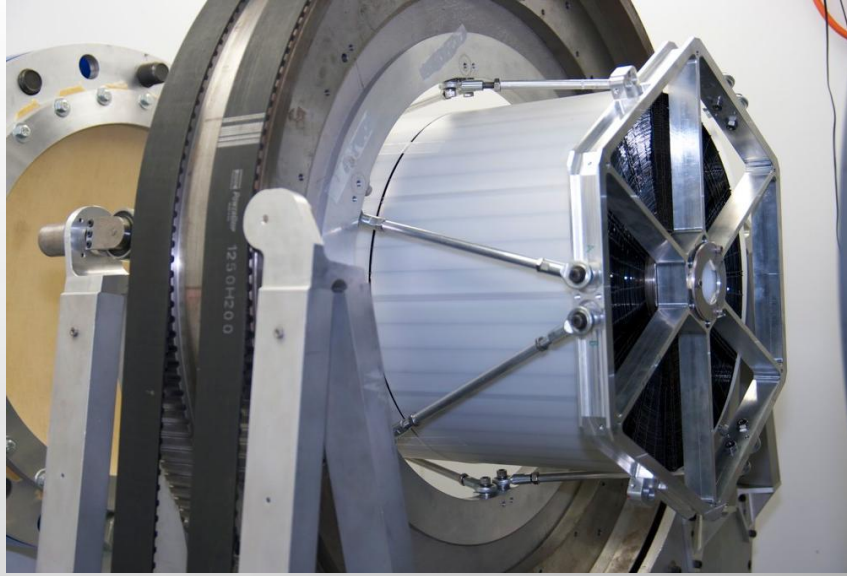


Optic with more than 100 layers

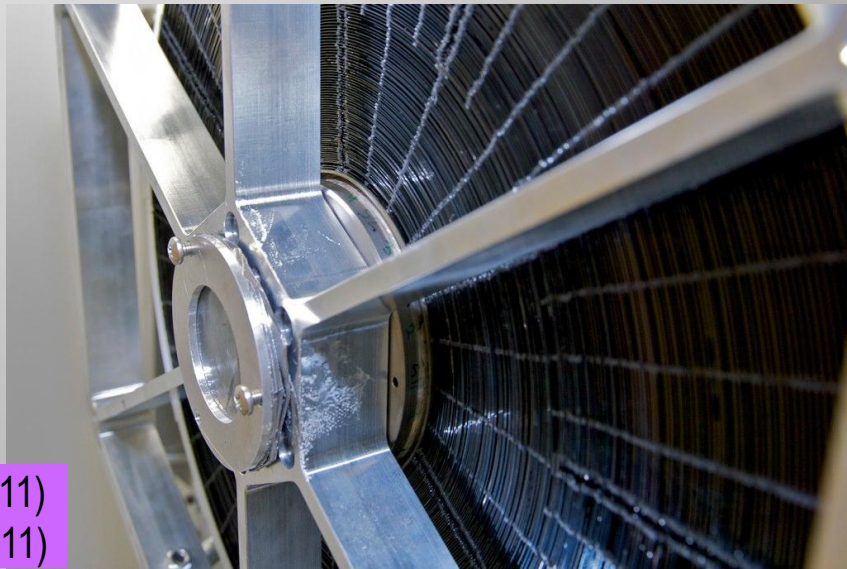
# NuSTAR telescope details

Focal Length	10.15 m
Shell Radii	51–191 mm
Graze Angles	0.074–0.224°
Shell Length	225 mm
Mirror Thickness	0.2 mm
Shells Per Module	130
Mirror Segments Per Module	2340

C Hailey et al. Proc SPIE ,7732, (2010)



J Koglin et al., Proc SPIE, 8147, (2011)  
 W Craig et al., Proc SPIE, 8147, (2011)



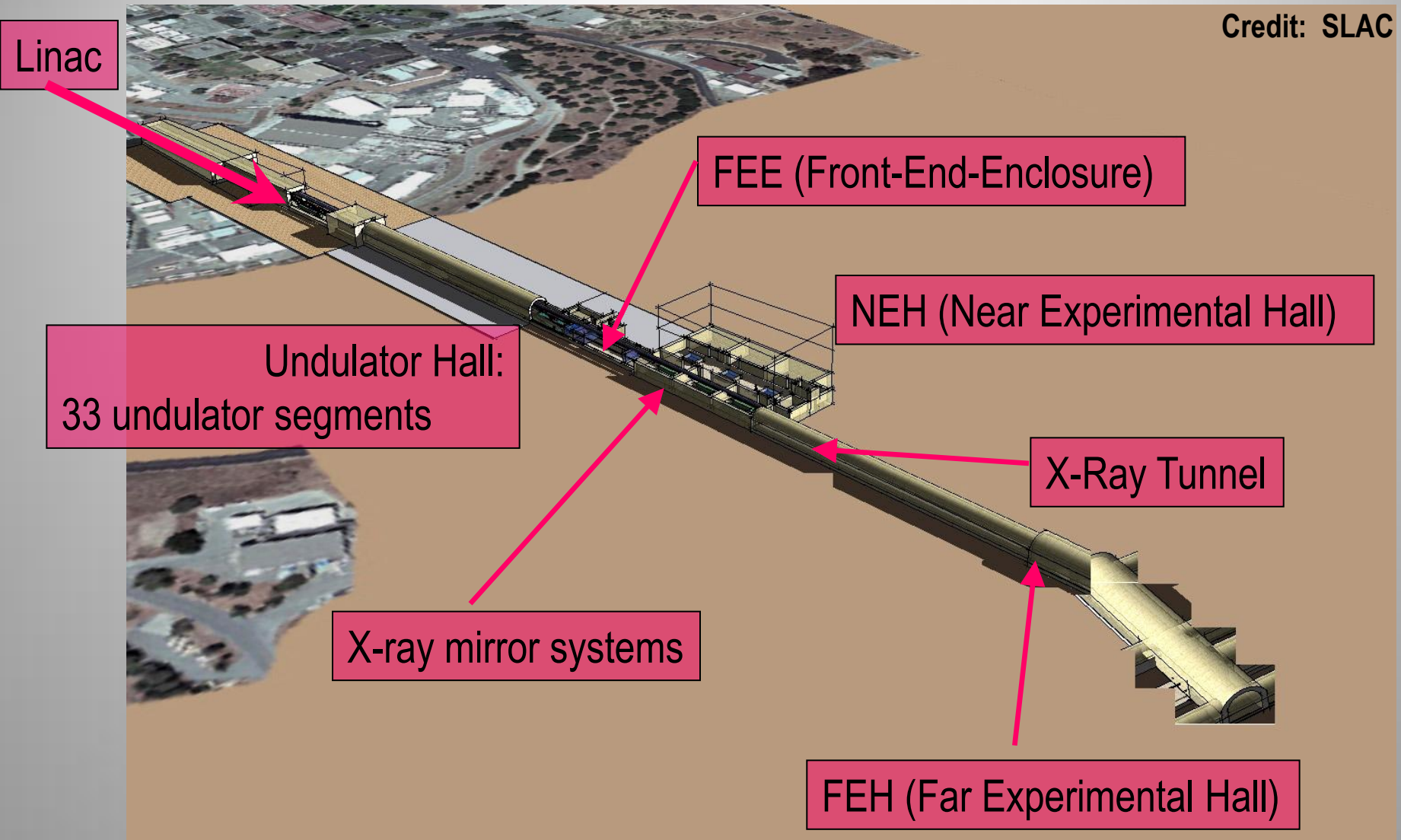


# LCLS X-RAY OFFSET MIRRORS



# Linac Coherent Light Source (LCLS) at SLAC

Credit: SLAC



# From the undulator hall to the users

- FEL (0.8-8 keV, 1<sup>st</sup> harmonic) comes with high-energy bremsstrahlung (spontaneous) emission that is both dangerous and contaminating
- To eliminate its presence, use a series of mirrors to filter out unwanted component, as well as deliver beam to different end stations

Parameter	0.827 keV	8.27 keV
FEL pulse (rms)	137 fs	73 fs
FEL width (FWHM)	81 $\mu\text{m}$	60 $\mu\text{m}$
FEL divergence (FWHM)	8.1 $\mu\text{rad}$	1.1 $\mu\text{rad}$
FEL brightness [ $\gamma \text{ s}^{-1} \text{ mm}^{-2} \text{ mrad}^{-2} (0.1\% \text{ bw})^{-1}$ ]	$0.28 \times 10^{32}$	$15 \times 10^{32}$
Avg FEL power	0.23 W	0.23 W
Avg Spontaneous power	0.24 W	2.2 W

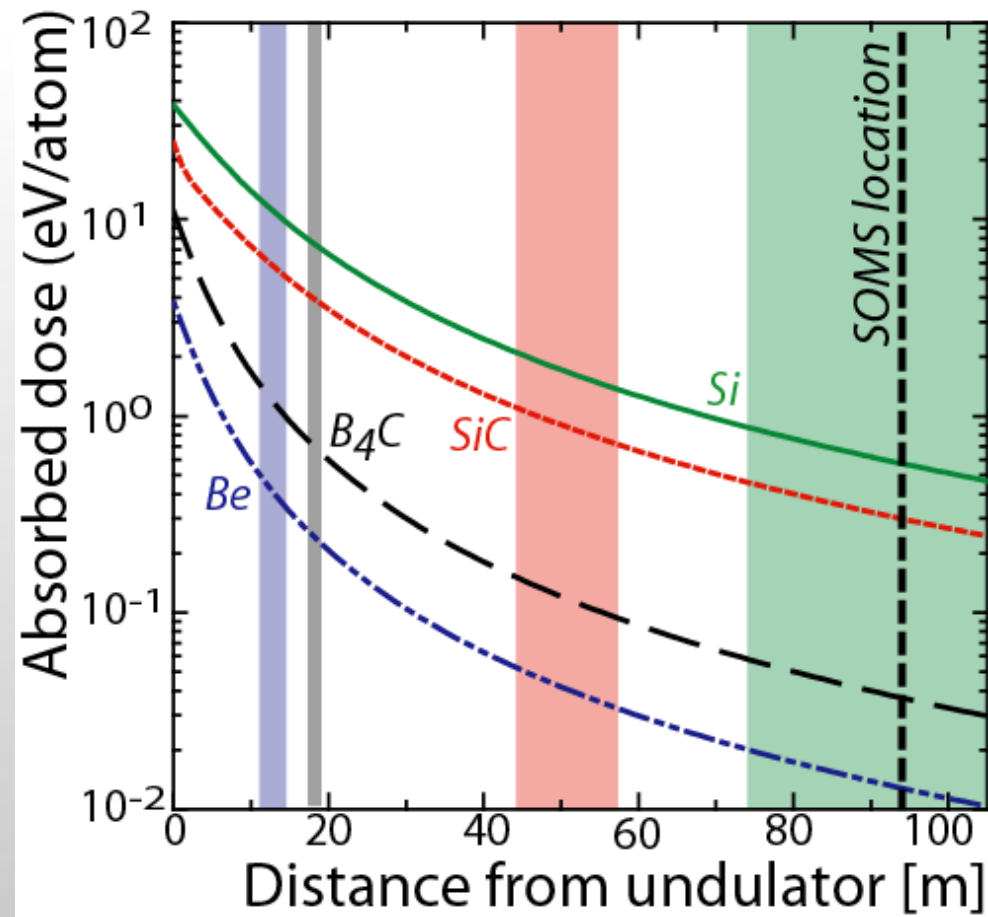
**Science driver: safely transport beam to End Stations with minimal loss of coherence or intensity and no damage to optics**

**Solution: X-ray mirrors made by depositing thin films on very smooth, very flat precision-fabricated silicon substrates**



# Damage considerations

- Consider doses for:
  - thermal fatigue ( $D_3$ ), reaching melt ( $D_2$ ), melting ( $D_1$ )
  - $D_1 > D_2 > D_3$
- Experiments at FLASH show damage occurs for  $D_1$ - $D_2$
- Vertical bands indicate where materials will become damaged
  - Must place elements made from materials to the right of the bands to prevent damage



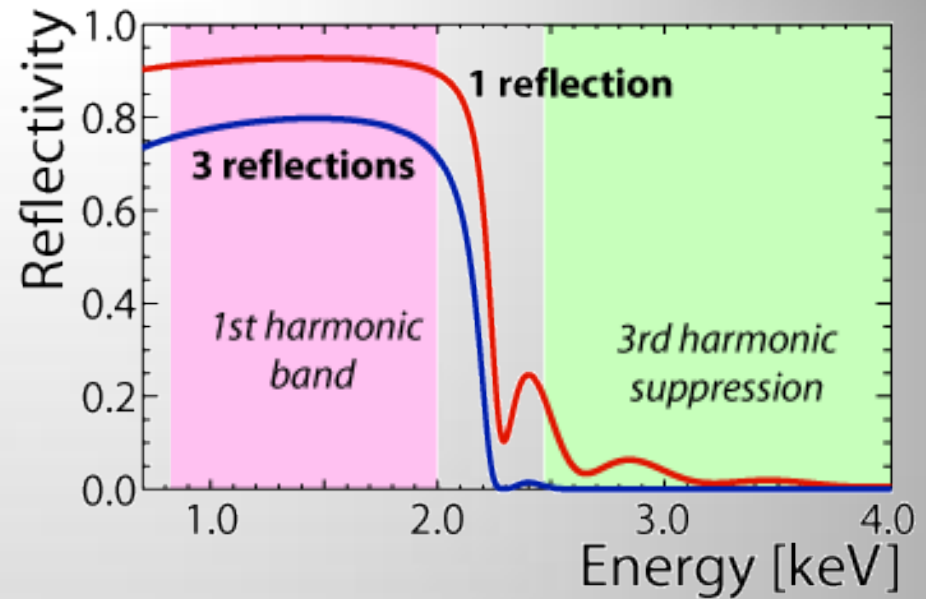
Plot courtesy of Stefan Hau-Riege (LLNL);  
S Hau-Riege et al., *Opt Express*, **18**, 23933, (2010)

Very few materials will survive the fully saturated FEL!

# Manufacturing approach for LCLS X-ray mirrors

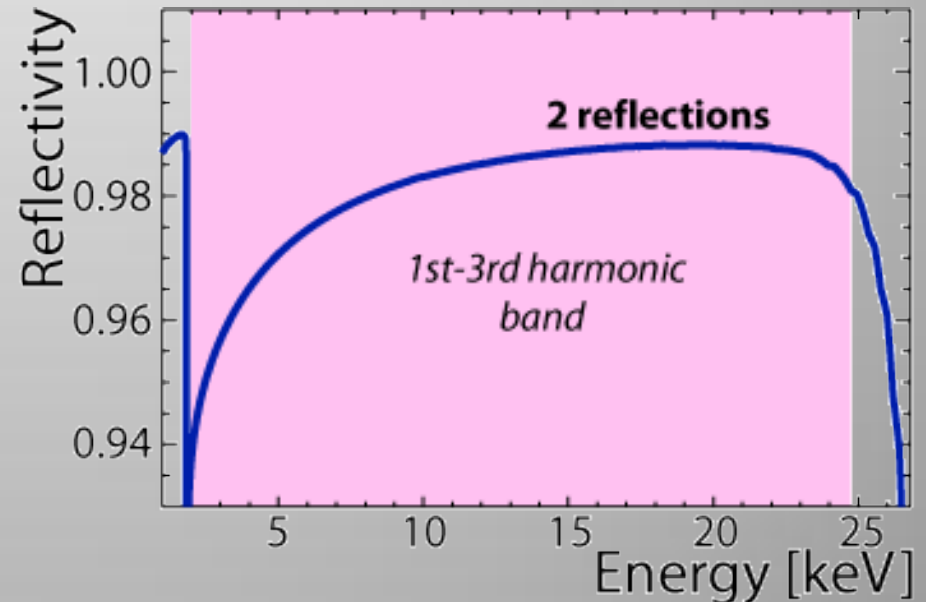
## For SOMS (0.8-2.0 keV): B<sub>4</sub>C

- Polish/figure B<sub>4</sub>C monolithic mirror: infeasible
- Procure Si substrate from commercial vendor, deposit 50-nm thick B<sub>4</sub>C reflective coating at LLNL

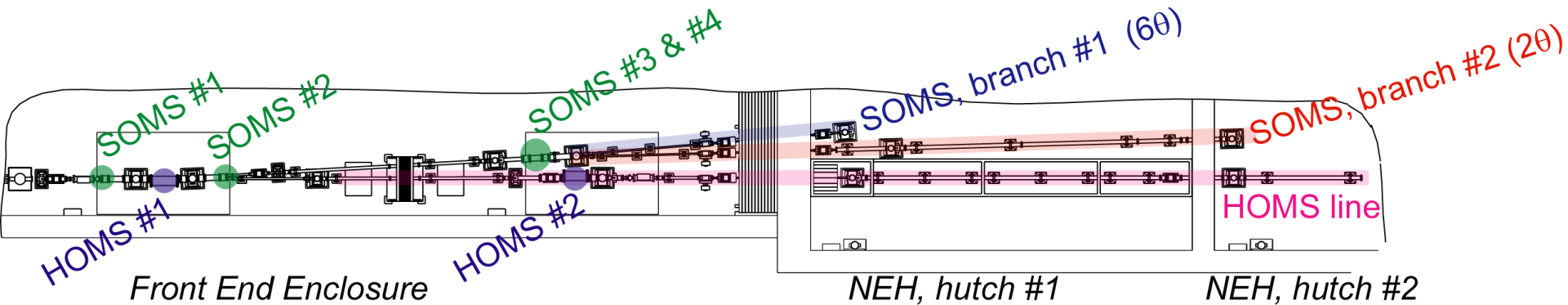


## For HOMS (2-25 keV): SiC

- Polish/figure SiC monolithic mirror: very challenging
  - Procure Si substrate from commercial vendor, deposit 50-nm thick SiC reflective coating at LLNL
- For both systems, ensure coatings, mounting and pointing do not degrade substrate quality



# Layout of mirror systems

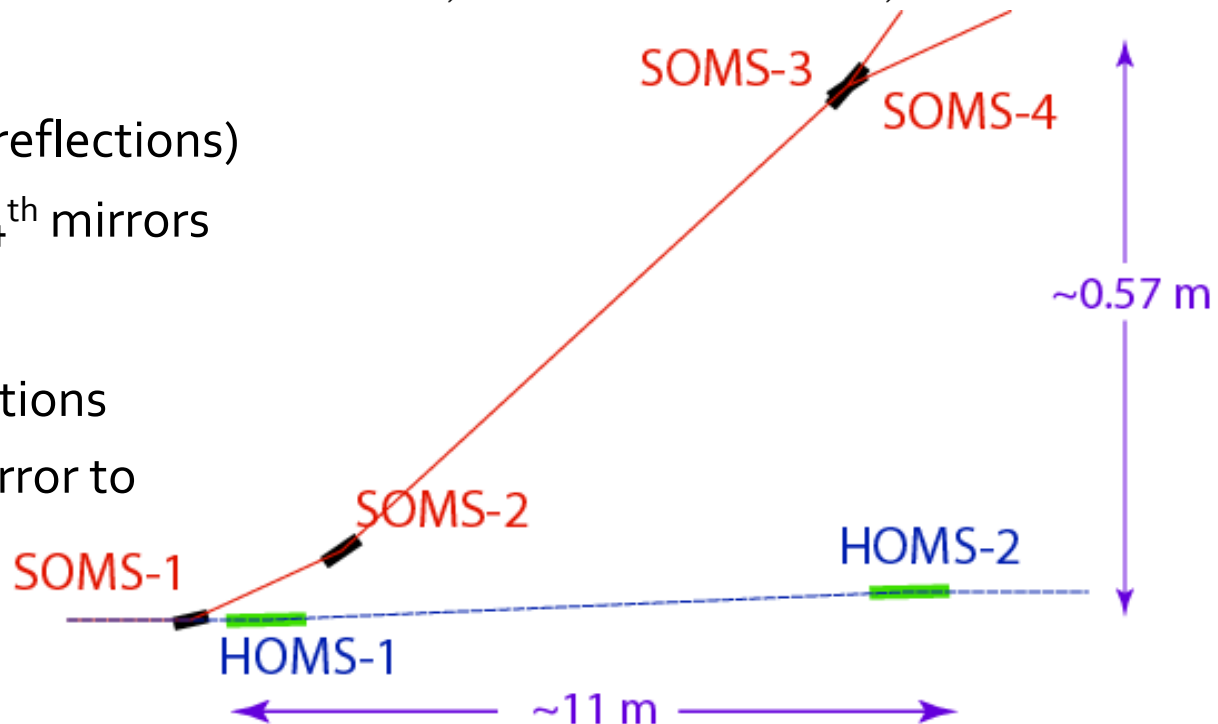


## SOMS: $0.8 < E < 2$ keV

- Total of four mirrors (3 reflections)
- Choose between 3<sup>rd</sup> & 4<sup>th</sup> mirrors

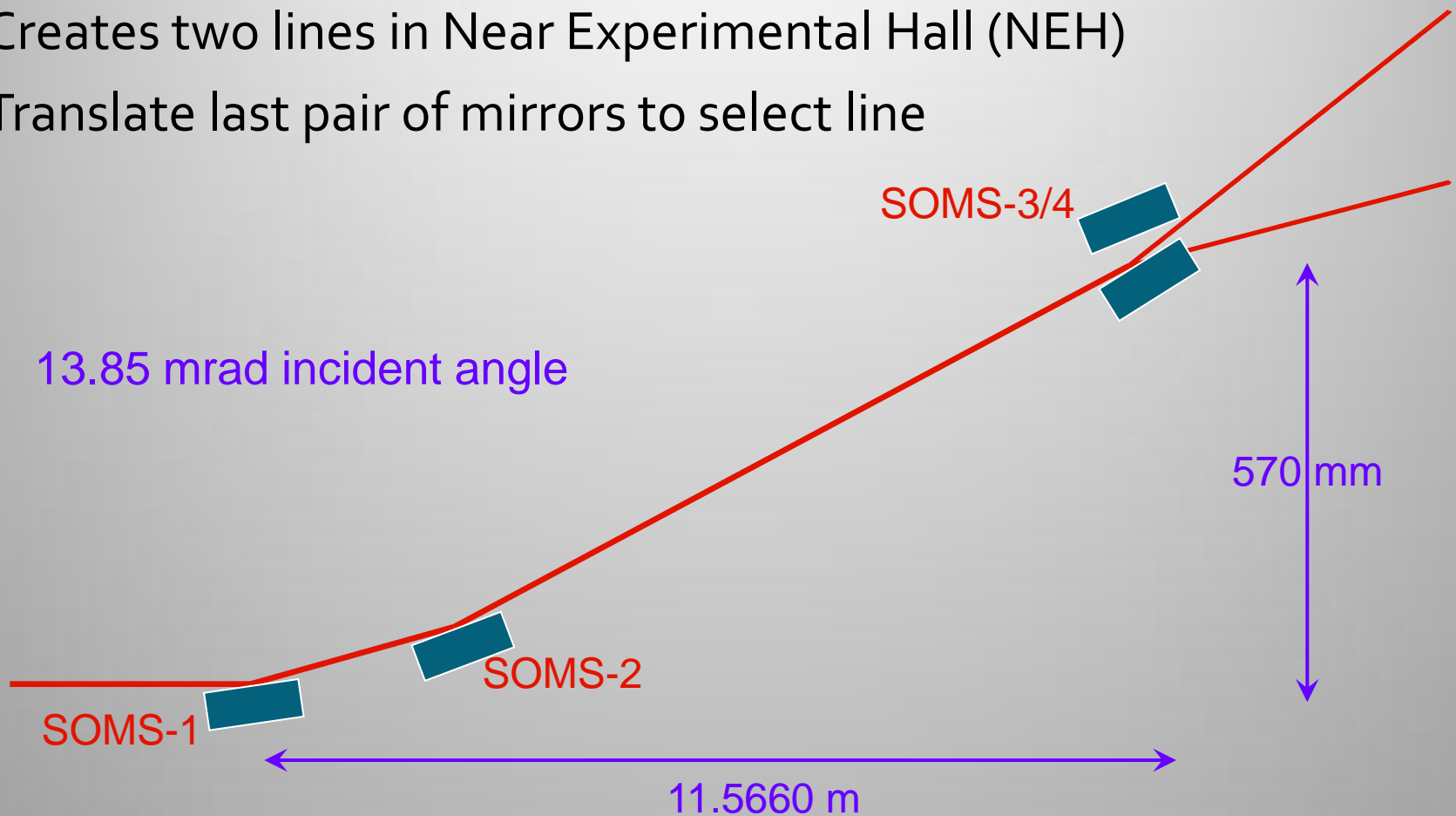
## HOMS: $2 < E < 24.8$ keV

- Two mirrors/two reflections
- Withdraw 1<sup>st</sup> SOMS mirror to access beamline



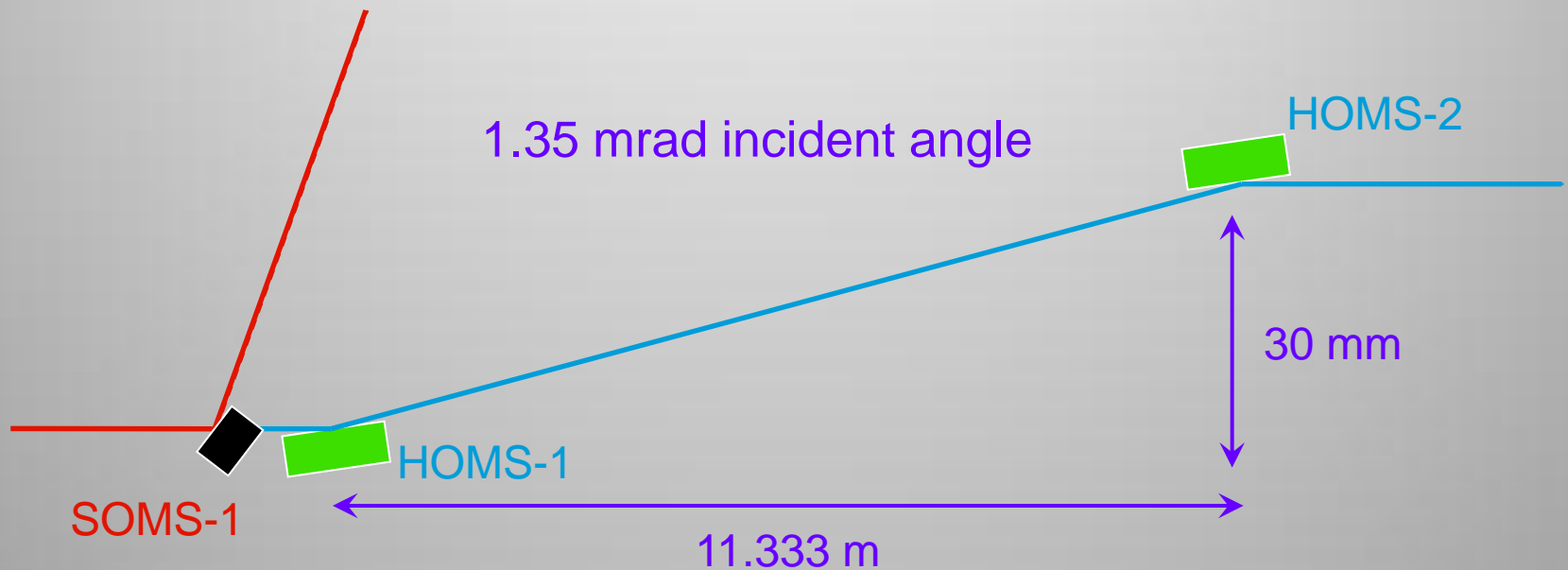
# SOMS: Soft X-ray offset mirror system

- Three reflection design to maximize horizontal deflections
- Creates two lines in Near Experimental Hall (NEH)
- Translate last pair of mirrors to select line



# HOMS: Hard X-ray offset mirror system

- Periscope design, 30 mm horizontal offset
- Withdraw first SOMS mirror to send hard beam to Fall Experimental Hall (FEH)





# Summary of LCLS x-ray mirror specifications

## Guiding design philosophy

- Maximize throughput (high reflectivity, sufficiently long mirrors)
- Limit increase in beam size
- Minimize wave-front distortions
- Balance against state of the art vendor capabilities
- Start with metrology data from recent mirrors delivered to SSRL; iterate with potential vendors to explore possibility for improvements
- Use formalism developed by Church & Takacs (and others)

**Balance requirements  
against manufacturability**

Error Category		Specification	Spatial Wavelength
Figure	Height Error	$\leq 2.0 \text{ nm rms}^\ddagger$	1 mm to Clear Aperture <sup>†</sup>
	Slope Error	$\leq 0.25 \text{ } \mu\text{rad rms}^\ddagger$	
Mid-Spatial Roughness		$\leq 0.25 \text{ nm rms}$	2 $\mu\text{m}$ to 1 mm
High-Spatial Roughness		$\leq 0.4 \text{ nm rms}$	20 nm to 2 $\mu\text{m}$

<sup>†</sup> SOMS mirrors: Flat, planar,  $250 \times 30 \times 50 \text{ mm}^3$ , Clear Aperture =  $175 \times 10 \text{ mm}^2$

<sup>†</sup> HOMS mirrors: Pseudo-planar\*\*,  $450 \times 30 \times 50 \text{ mm}^3$ , Clear Aperture =  $385 \times 15 \text{ mm}^2$

\*\*Substrate ground curved, and then bent flat

<sup>‡</sup>limited by manufacturers' capabilities

M. Pivovarov *et al.*, *Proc SPIE*, **6705**, (2007)



# Reflective coating requirements for LCLS X-ray mirrors

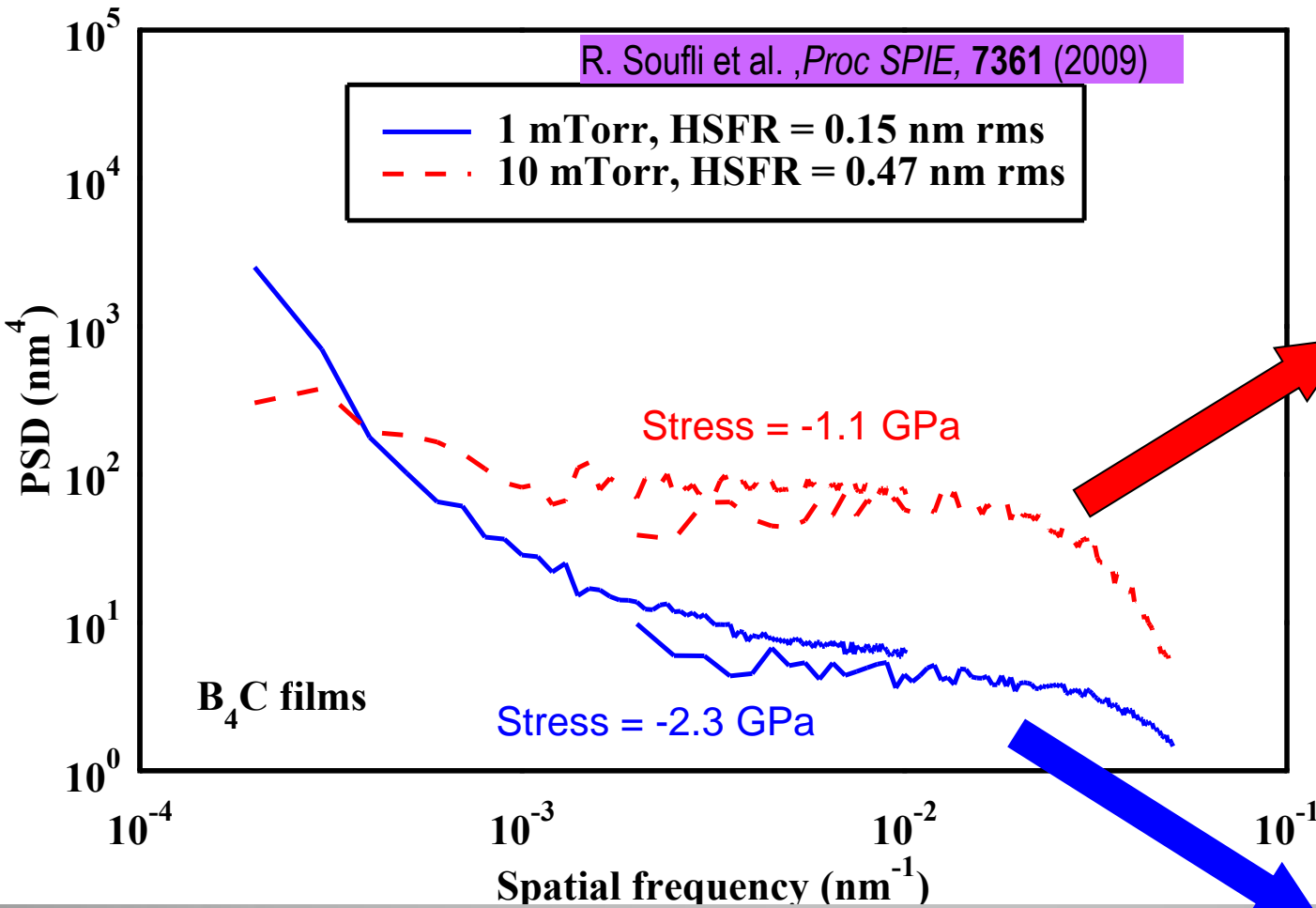
- Figure: Coating should preserve the substrate figure specification of  $0.25 \mu\text{rad rms}$  &  $2 \text{ nm rms}$   $\sigma_{\text{total}}^2 = \sigma_{\text{sub}}^2 + \sigma_{\text{film}}^2$
- ➔ Coating is allowed to contribute  $< 1 \text{ nm rms}$  figure error across clear aperture ( $175 \times 10 \text{ mm}^2$  for SOMS,  $385 \times 5 \text{ mm}^2$  for HOMS)
- Roughness: Coating should have low HSFR (will inherently replicate MSFR)
- Stress: Coating should have low stress ( $< 1 \text{ GPa}$  for  $\sim 50 \text{ nm}$  coating thickness), to prevent figure deformation or delamination from Si substrate
- Lifetime stability: Coating should be stable over time in ambient conditions, and under the operating conditions of LCLS X-ray mirror system

“Mag 4” magnetron sputtering tool can accommodate 450 mm long substrates

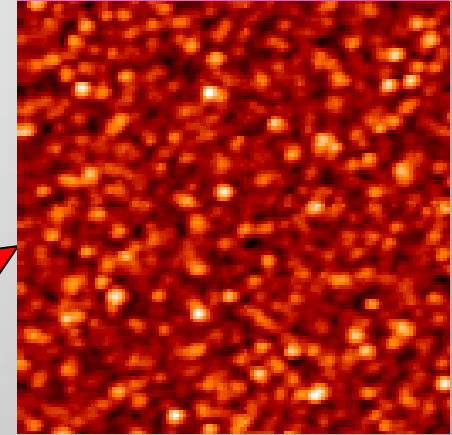


Underneath view of LLNL chamber lid with 5 sputtering targets

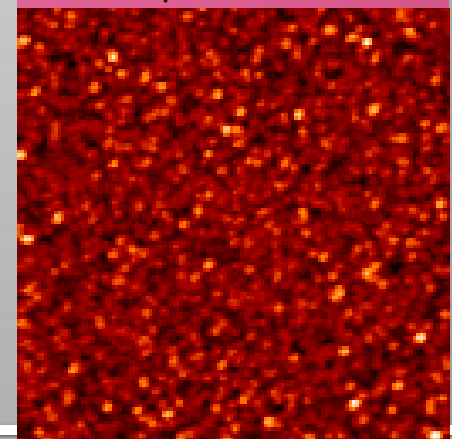
# Boron carbide thin film development for LCLS SOMS mirrors



500×500  $nm^2$  detail from  
2x2  $\mu m^2$  AFM scan



500×500  $nm^2$  detail from  
2x2  $\mu m^2$  AFM scan



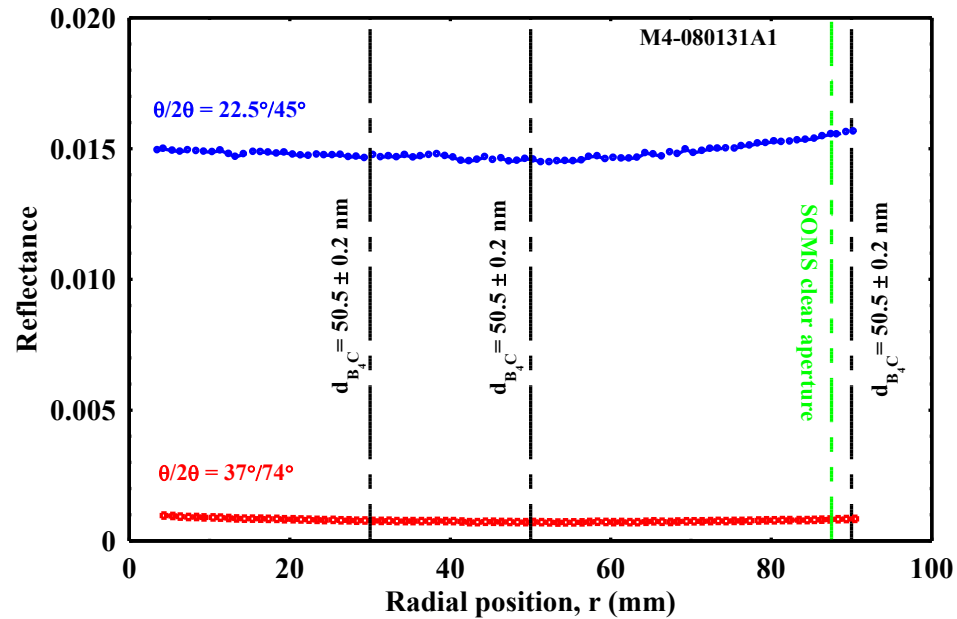
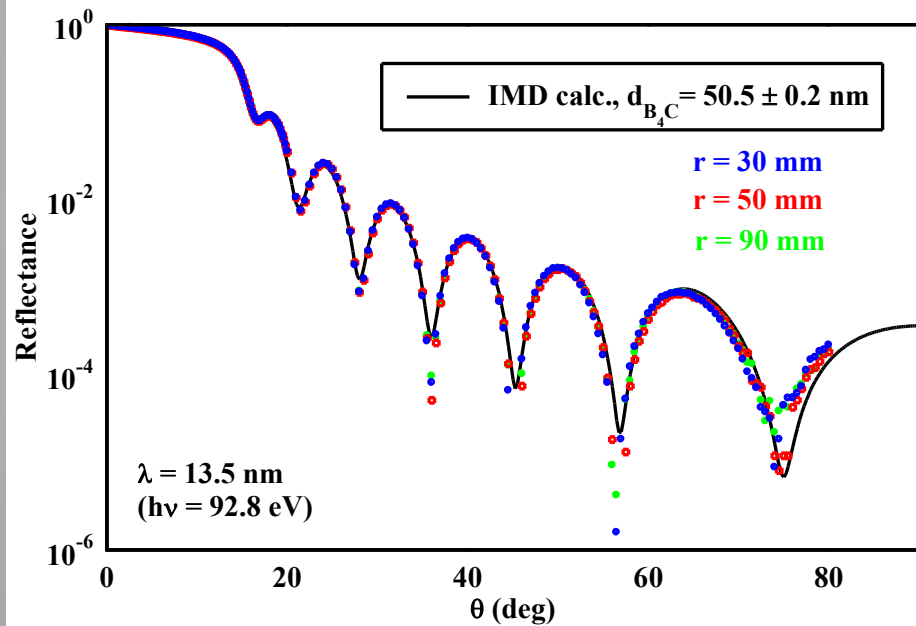
$$\sigma^2 = 2\pi \int_{f_1}^{f_2} f S(f) df$$

where  $S(f) \equiv PSD (nm^4)$ ,  $f_1 = 5 \times 10^{-4} nm^{-1}$ ,  $f_2 = 5 \times 10^{-2} nm^{-1}$



# SOMS and HOMS coating thickness uniformity is well within 1 nm rms specification

Measurements obtained at ALS beamline 6.3.2. (LBNL)



R. Soufli *et al.*, *Proc SPIE*, 7077, (2008)

- $B_4C$  measured thickness variation:  $< 0.4$  nm P-V,  $< 0.14$  nm rms ( $< 0.28\%$  rms) across the 175-mm SOMS clear aperture
- SiC measured thickness variation:  $< 1$  nm P-V,  $< 0.34$  nm rms ( $< 0.7\%$  rms) across the 385-mm HOMS clear aperture



# HOMS and SOMS engineering challenges

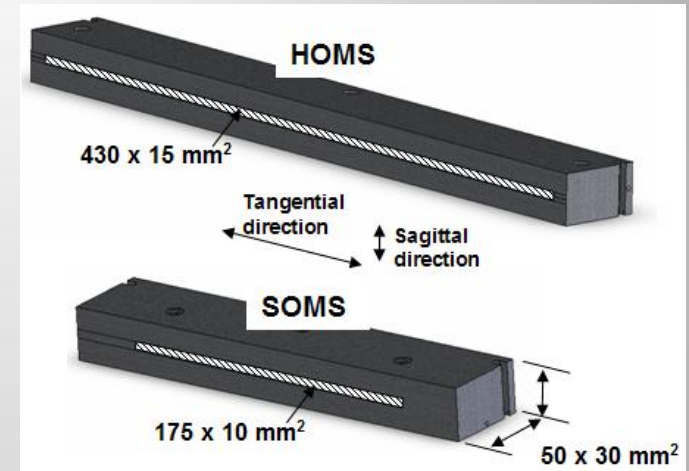
- Pointing
  - Facility requirement of less than 10% increase in spot size
    - SOMS < 900 nrad
    - HOMS < 90 nrad
- Flatness requirements
  - Ideally, better than 1 nm rms height errors for coherence preservation
  - High-stress coatings will impart spherical curvature—manufacturer with concave bend to compensate
  - Ensure bending can remove spherical curvature induced by coatings
  - Design a mounting system that imparts minimal change to mirror
- Design for thermal and vibrational stability



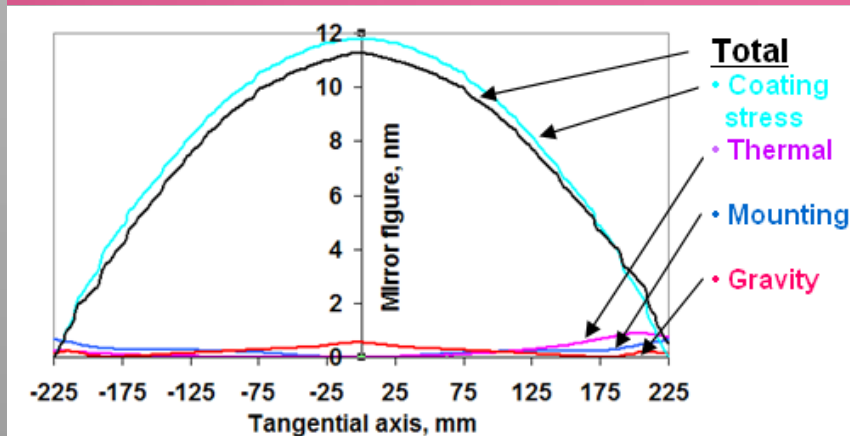
# The mirror & mount are designed to meet figure-error budget

To limit intensity ellipticity to 10%

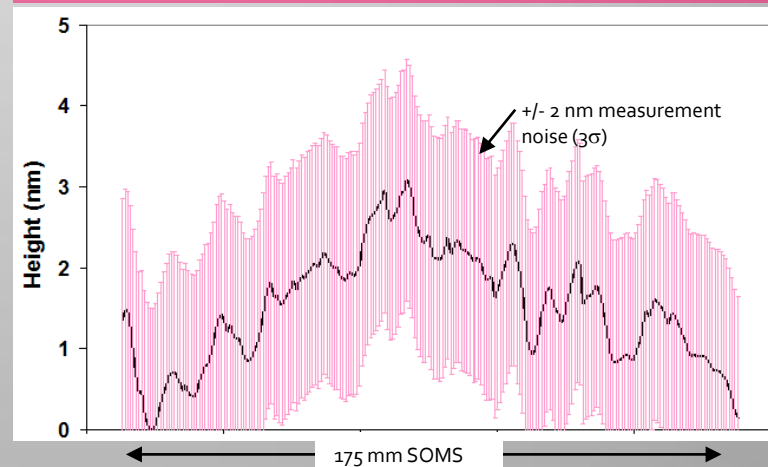
Requirement (sphere)		Figure error budget (sphere), nm				
Direction	Peak to Valley, nm	Mounting	Thermal	Coating stress	Gravity	Fabrication
HOMS/SOMS Sagittal	< 5		<< 1			<1
SOMS Tangential	<20	<1	<1.5	<4	<-1	<10
HOMS Tangential	<9	<1.5	<1.5	<12	<-1	<20



Finite element analysis guided optimization of the mirror and mount design (HOMS case is plotted);  
Analysis was benchmarked to measurements

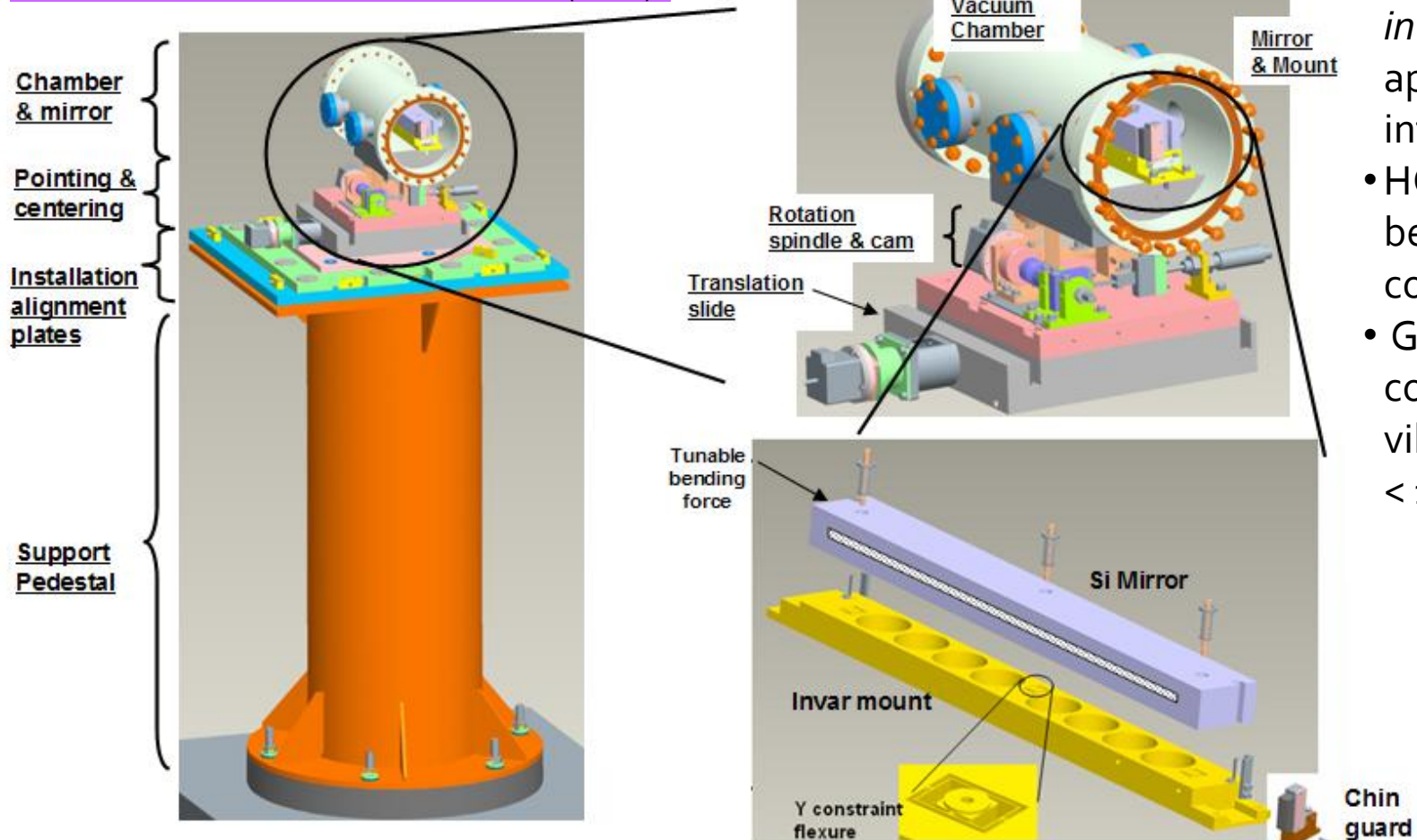


Coated SOMS measured every 2 min for 48 hr  
12"-aperture interferometer calibrated with 3-flat test



# HOMS and SOMS installation and alignment at LCLS

T. J. McCarville *et al.*, *Proc SPIE*, 7077, (2008)



- Mounting employs flexures
- Adjust, based on *in situ* full-aperture interferometry
- HOMS figure can be remotely controlled
- Good design controls vibrational jitter < 10 nrad

- Thermal stability for rotation/translation is 70/300 nrad/0.1° C
- T-controlled enclosure demonstrates  $\pm 0.01$  °C temperature and  $\pm 30$  nrad HOMS stability

# HOMS #1 figure coated and installed on mount

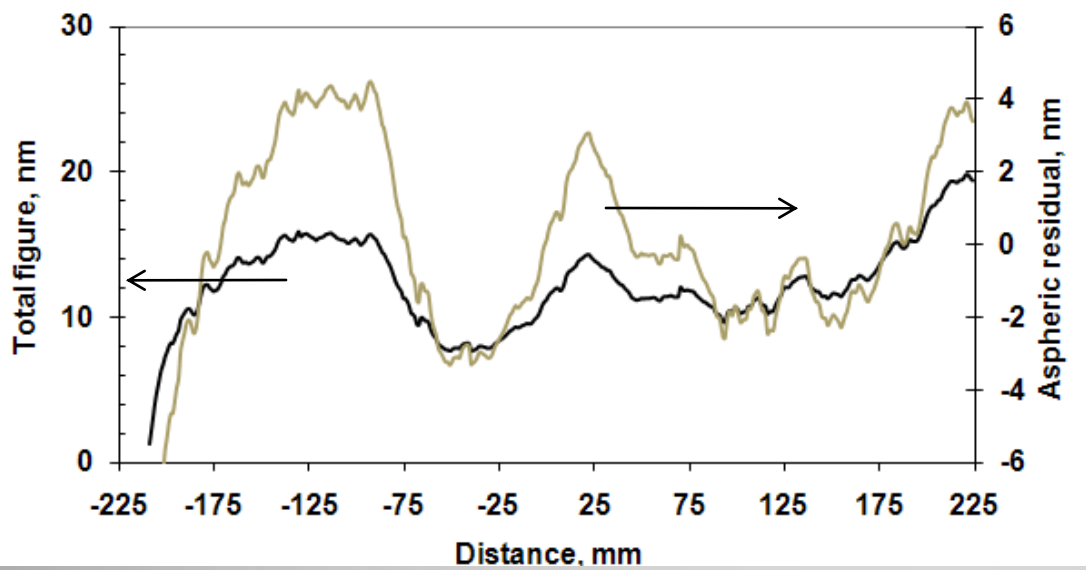
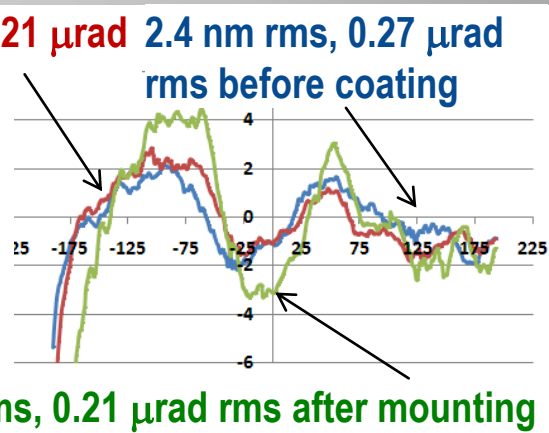
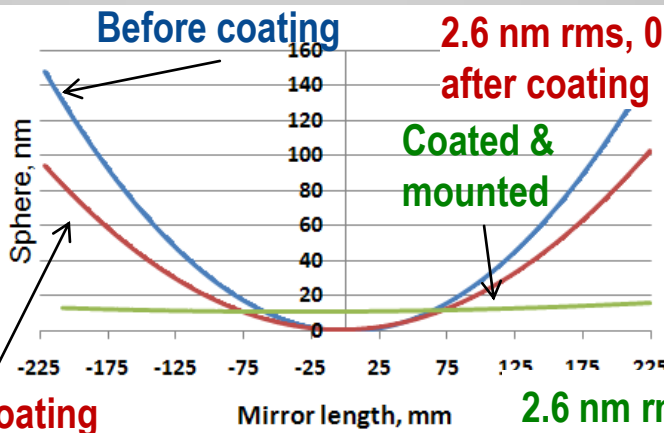
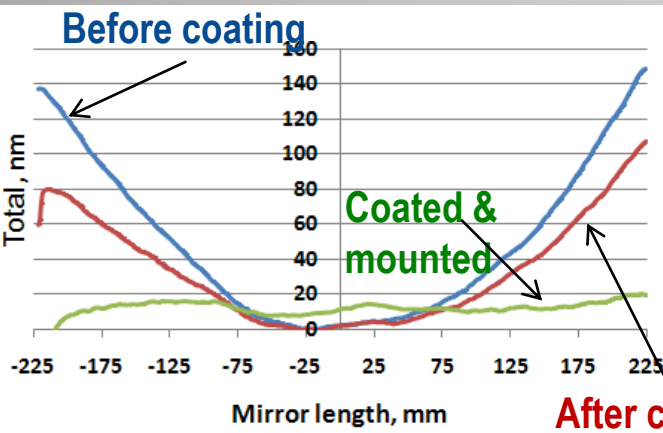


Figure corrections have been made to HOMS mounted mirrors without significantly contributing to aspheric curvature

Total figure = Spherical curvature + Aspheric residual



2.6 nm rms, 0.21  $\mu$ rad 2.4 nm rms, 0.27  $\mu$ rad

after coating

rms before coating

Coated & mounted

2.6 nm rms, 0.21  $\mu$ rad rms after mounting



# HOMS #2 figure coated and installed on mount

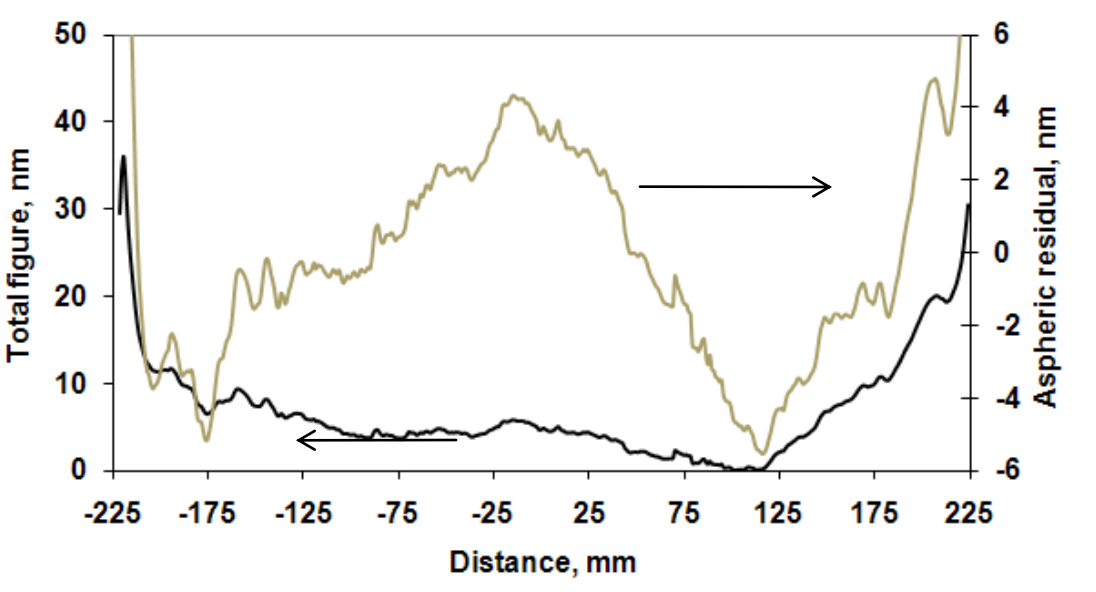
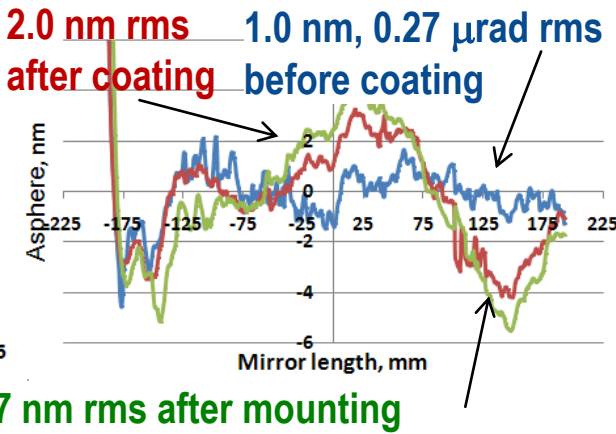
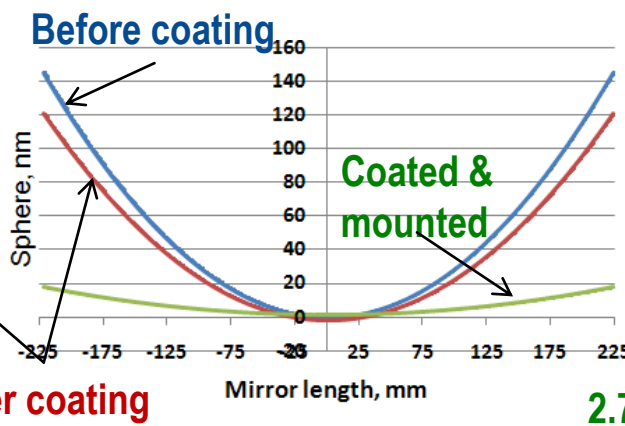
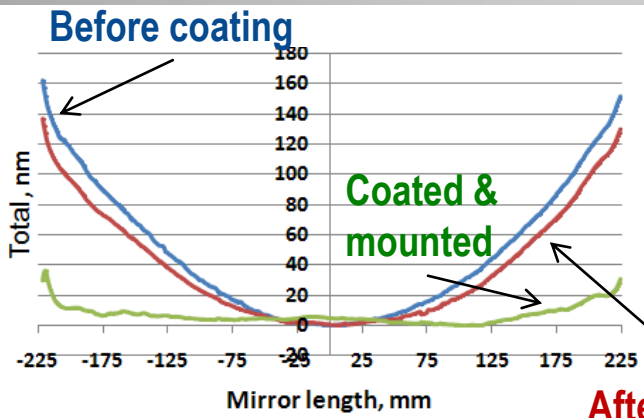


Figure corrections have been made to HOMS mounted mirrors without significantly contributing to aspheric curvature

Total figure = Spherical curvature + Aspheric residual

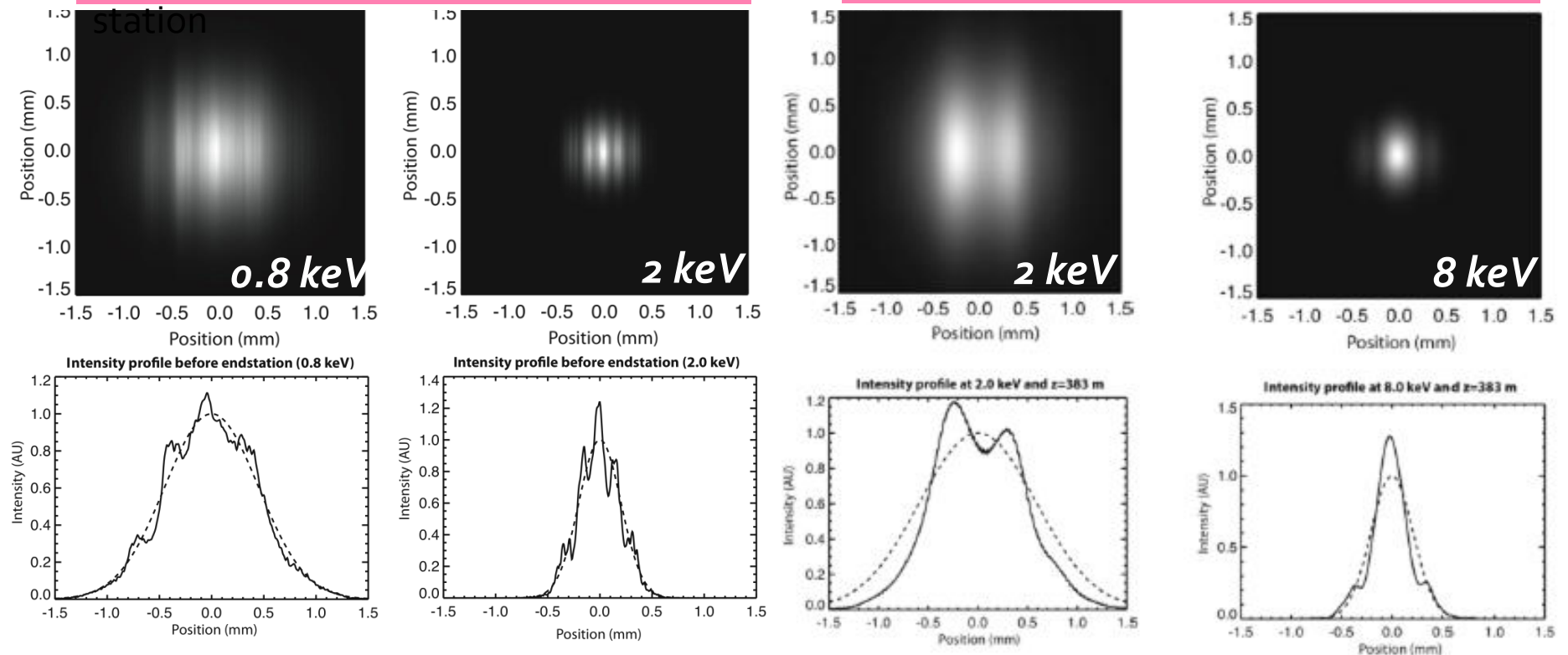


# SOMS & HOMS performance predictions

- LLNL metrology data, coupled into coherent wavefront propagation code, used to predict HOMS & SOMS focal spot structure
  - Scalar diffraction model was employed
  - Same methodology to select order of SOMS and HOMS elements for optimum performance

SOMS branch line before AMO end

HOMS branch line before CXI end



# FUTURE TRENDS



# X-ray astronomy

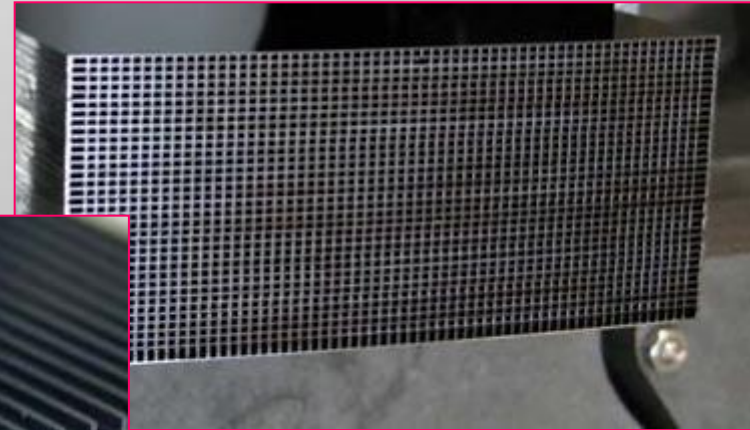
- ESA (and NASA?) pursuing large missions



- ESA now pursuing L-class mission ATHENA (Advanced Telescope for High ENergy Astrophysics)

- Technologies

- Silicon pore optics
- Slumped glass
- Replication ?

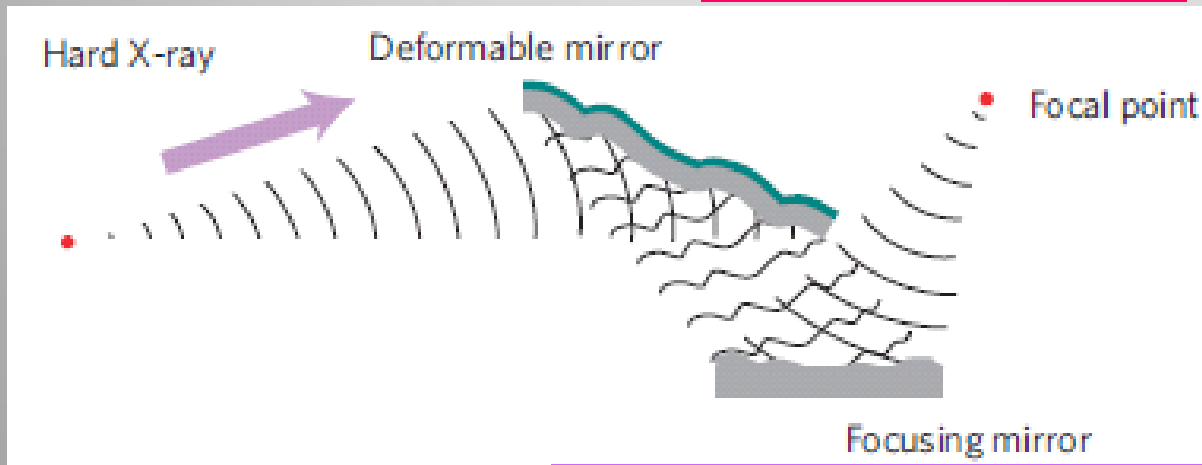


Marcos Bavdaz, "Silicon Pore Optics", (MPE: 17-19 Sep 2008)

# Adaptive x-ray optics

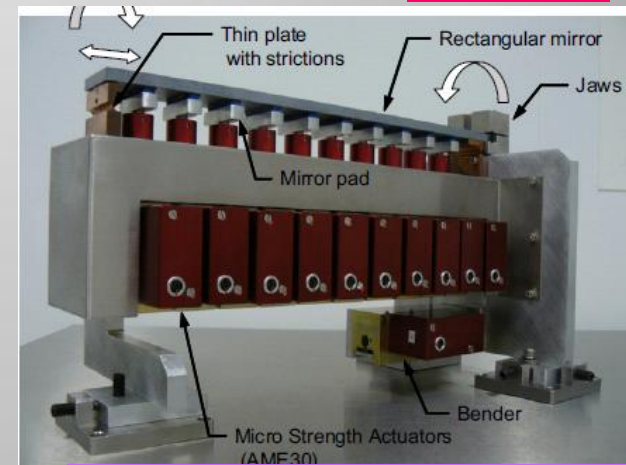
- Light sources will place ever more stringent requirements on optics
- Traditional fabrication and metrology approaches may not work
- One approach: closed-loop, *in situ* monitoring (e.g., using at-wavelength sensing) and correction using actuated mirrors
- Some state-of-the-art efforts:

## Osaka consortium



H. Mimar et al., *Nat Phys*, **6**, 123, (2010)

## SOLEIL



M Idir et al., *NIM A*, **616**, 162, (2010)

- LLNL has a nascent effort underway that leverages strong visible light AO expertise and LCLS x-ray optics development effort